

BIOSKINS: Metamodels for a system of fibres

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Alessandro Bottaro

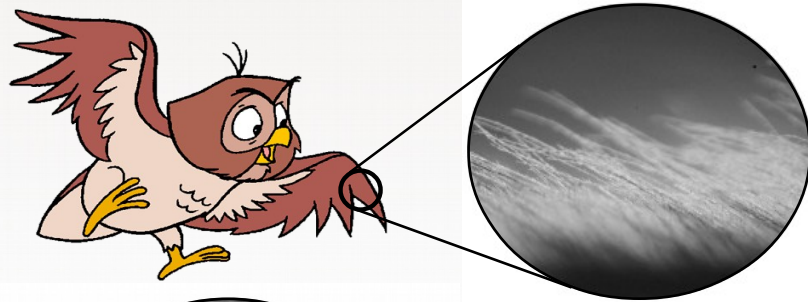
Toulouse, 14 Septembre 2017

PRESENTATION PLAN

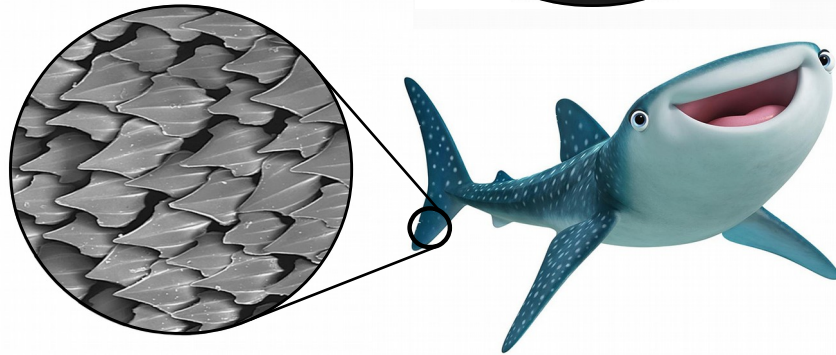
- Introduction
- VANS theory
- CFD: procedure and results
- DACE
- Metamodelling
- Kriging results
- Conclusions



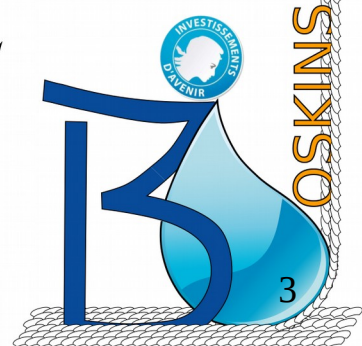
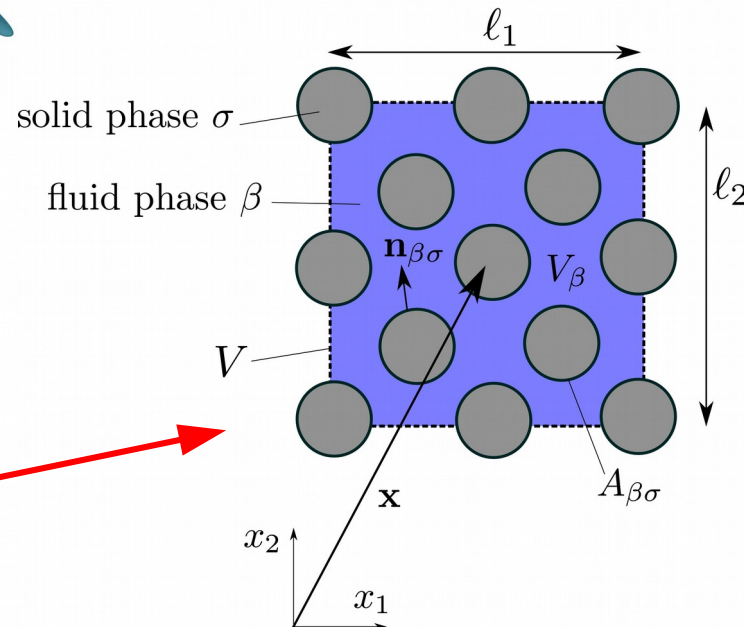
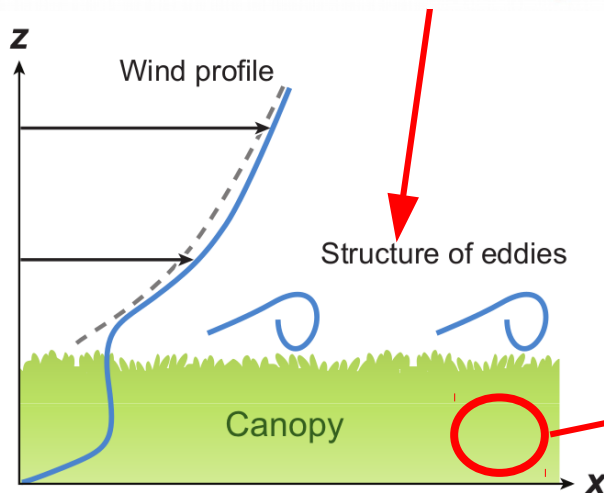
INTRODUCTION



The goal is to find a cheap way to **model poroelastic surfaces**



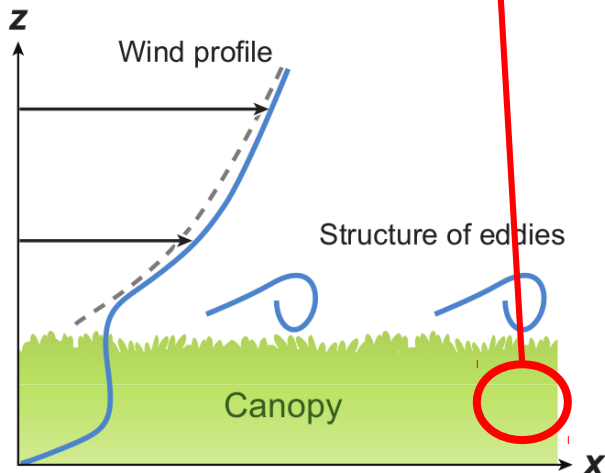
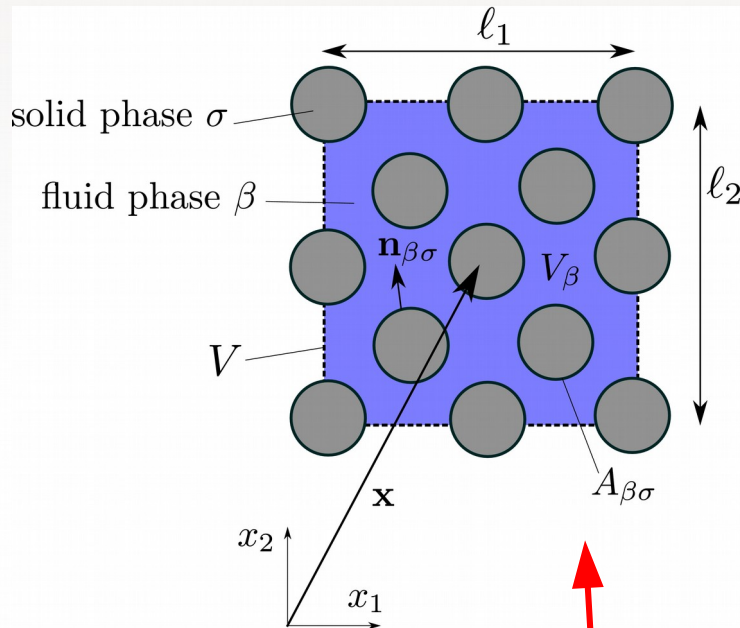
- The are many problems involved:
- Multiple scales
 - Interface coupling
 - Fluid structure interaction
 - Anisotropy



[Luminari, Airiau and Bottaro, "Drag-model sensitivity of Kelvin-Helmholtz waves in canopy flows", *Physics of fluids*, 2016]

VANS THEORY: 1

REV: Representative Elementary Volume



3D incompressible flow

$$\frac{\partial v}{\partial t} + v \cdot \nabla v = -\frac{1}{\rho} \nabla p + \nu \nabla^2 v$$

$$\nabla \cdot v = 0$$

1) Intrinsic **average** operator:

$$\langle \psi_\beta \rangle^\beta = \frac{1}{V_\beta} \int_{V_\beta} \psi(x) dV_\beta$$

2) Porosity:

$$\varepsilon = \frac{V_\beta}{V}$$

3) Field decomposition:

$$\psi = \langle \psi \rangle^\beta + \tilde{\psi}$$



VANS THEORY: 2

Applying 1) 2) and 3) to the NS system we obtain the VANS:

$$\frac{\partial \langle \mathbf{v}_\beta \rangle^\beta}{\partial t} + \langle \mathbf{v}_\beta \rangle^\beta \cdot \nabla \langle \mathbf{v}_\beta \rangle^\beta = -\frac{1}{\rho_\beta} \nabla \langle p_\beta \rangle^\beta + \nu_\beta \nabla^2 \langle \mathbf{v}_\beta \rangle^\beta + \frac{1}{V_\beta} \int_{A_{\beta\sigma}} \left(-\frac{\tilde{p}_\beta}{\rho_\beta} \mathbf{I} + \nu_\beta \nabla \tilde{\mathbf{v}}_\beta \right) \cdot \mathbf{n}_{\beta\sigma} dA$$

$$\nabla \cdot \langle \mathbf{v}_\beta \rangle^\beta = 0$$

The fluctuations are still in the equation

4) A closure model is required

micro \rightarrow

$$\mathbf{D} = \frac{1}{V_\beta} \int_{A_{\beta\sigma}} \left(-\frac{\tilde{p}_\beta}{\rho_\beta} \mathbf{I} + \nu_\beta \nabla \tilde{\mathbf{v}}_\beta \right) \cdot \mathbf{n}_{\beta\sigma} dA$$

MACRO \rightarrow

$$-\nu_\beta \varepsilon \mathbf{K}^{-1} (\mathbf{I} + \mathbf{F}) \langle \mathbf{v}_\beta \rangle^\beta$$

Permeability tensor \mathbf{K} Forchheimer tensor \mathbf{F}



CLOSURE PROBLEMS

$$\left\{ \begin{array}{l} 0 = -\nabla \mathbf{d} + \nabla^2 \mathbf{D} + \mathbf{I} \\ \nabla \cdot \mathbf{D} = 0 \\ \mathbf{D} = 0 \quad \text{at} \quad A_{\beta\sigma} \\ \mathbf{d}(\mathbf{x} + \ell_i) = \mathbf{d}(\mathbf{x}), \quad \mathbf{D}(\mathbf{x} + \ell_i) = \mathbf{D}(\mathbf{x}) \quad i = 1, 2, 3 \end{array} \right. \quad \text{STOKES REGIME}$$

$$\varepsilon \langle \mathbf{D} \rangle^i = \mathbf{K}$$

Thanks to the unity matrix the equations are decoupled with triplets (3x3 equations instead of 9 coupled)

The 3x3 systems have the structure of a Stokes, and Linearized Navier-Stokes problems (we can use the same numerical solvers)

In this case we need also the DNS microscopic field.

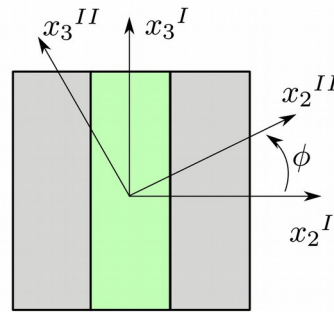
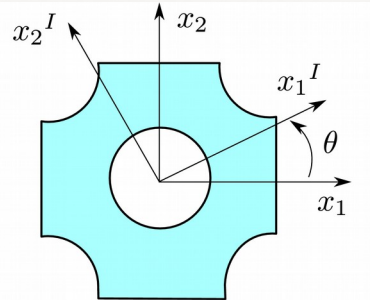
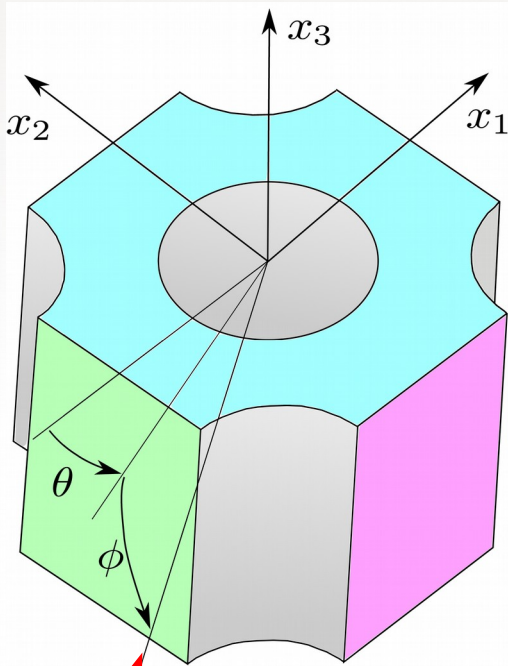
The two tensors depend on 4 different flow parameters

$$\left\{ \begin{array}{l} \frac{1}{\nu_\beta} \mathbf{v}_\beta \cdot \nabla \mathbf{M} = -\nabla \mathbf{m} + \nabla^2 \mathbf{M} + \mathbf{I} \\ \nabla \cdot \mathbf{M} = 0 \\ \mathbf{M} = 0 \quad \text{at} \quad A_{\beta\sigma} \\ \mathbf{m}(\mathbf{x} + \ell_i) = \mathbf{m}(\mathbf{x}), \quad \mathbf{M}(\mathbf{x} + \ell_i) = \mathbf{M}(\mathbf{x}) \quad i = 1, 2, 3 \end{array} \right. \quad \text{INERTIA REGIME}$$

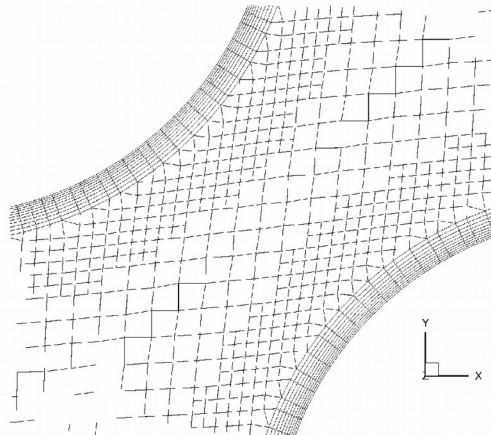
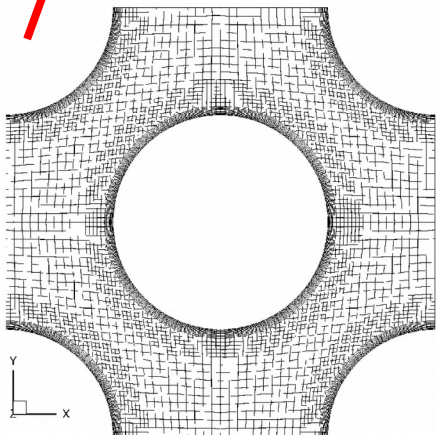
$$\varepsilon \langle \mathbf{M} \rangle^i = \mathbf{H}$$

$$\mathbf{H}^{-1} = \mathbf{K}^{-1} (\mathbf{F} + \mathbf{I}) \quad \Rightarrow \quad \mathbf{F} = \mathbf{K} \mathbf{H}^{-1} - \mathbf{I}$$

CFD PROCEDURE



f



Rigid cylindric filaments in staggered arrangements.

Imposing Re(through f), θ , ϕ , ε

Solve DNS with cyclic b.c.:

$$\frac{\partial \mathbf{v}_\beta}{\partial t} + \nabla \cdot (\mathbf{v}_\beta \mathbf{v}_\beta) = -\frac{1}{\rho} \nabla p_\beta + \nu_\beta \nabla^2 \mathbf{v}_\beta + \mathbf{f}$$

$$\nabla \cdot (\mathbf{v}_\beta) = 0$$

Solve closure problem (form previous slides).

Perform the averaging to obtain the 9 components of \mathbf{H} .

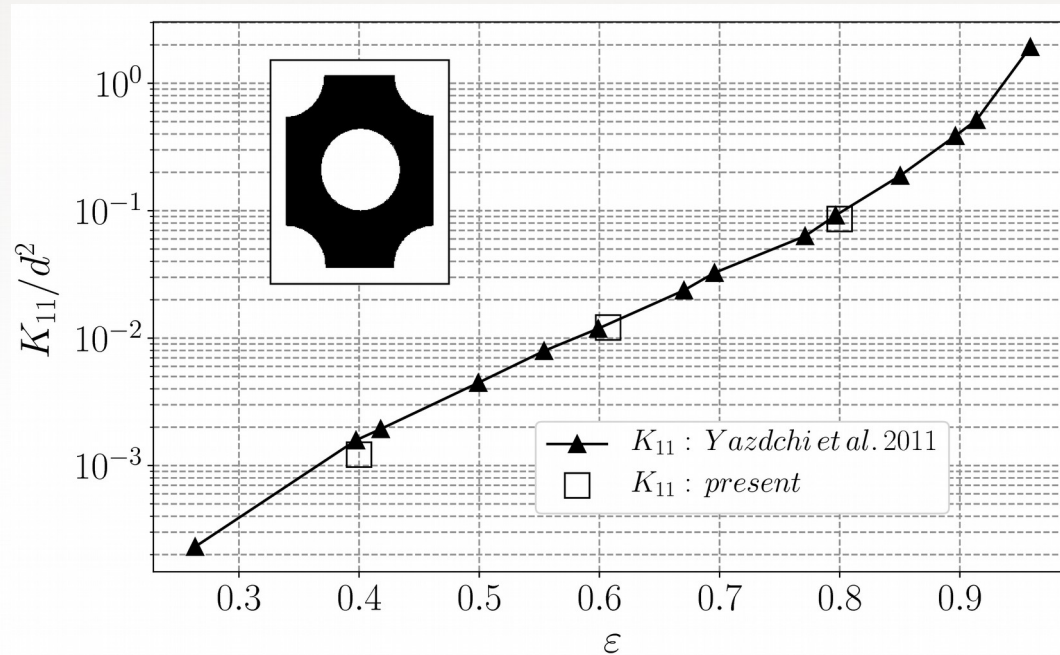
OpenFOAM

The Open Source CFD Toolbox

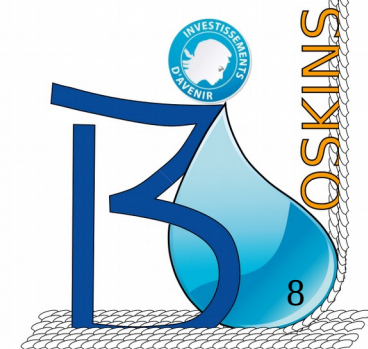
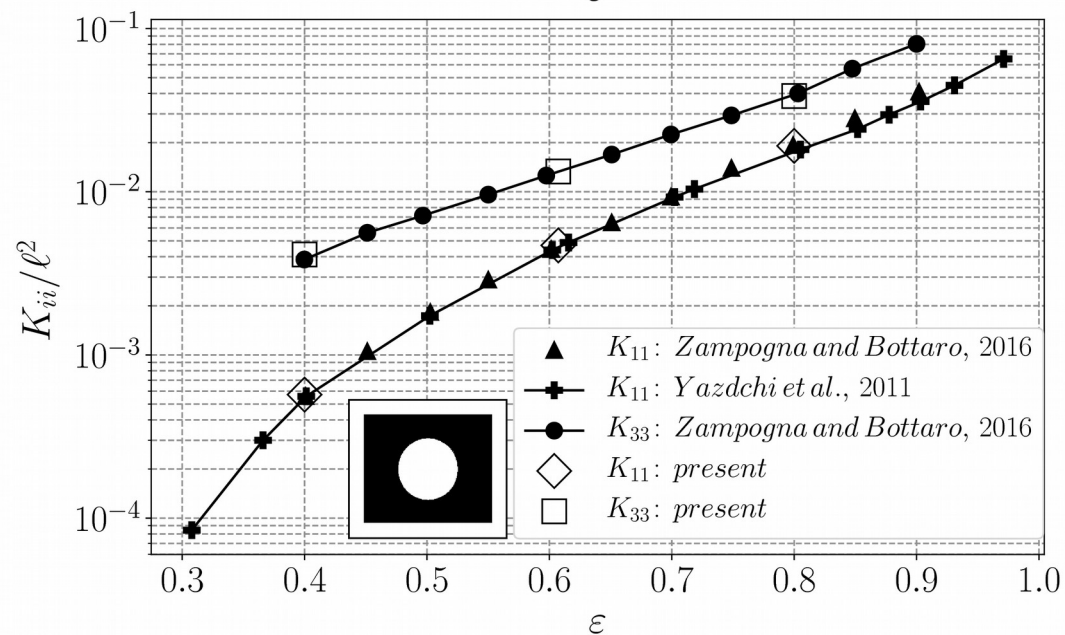


VALIDATION

Staggered
cylinder
arrangement



Centered
cylinder
arrangement



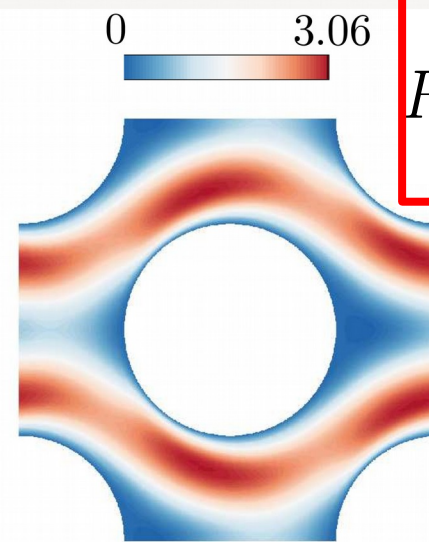
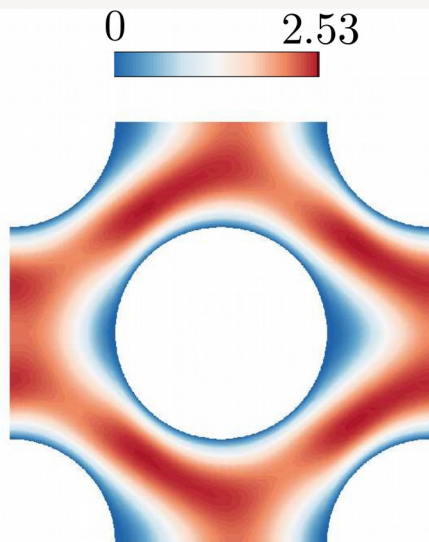
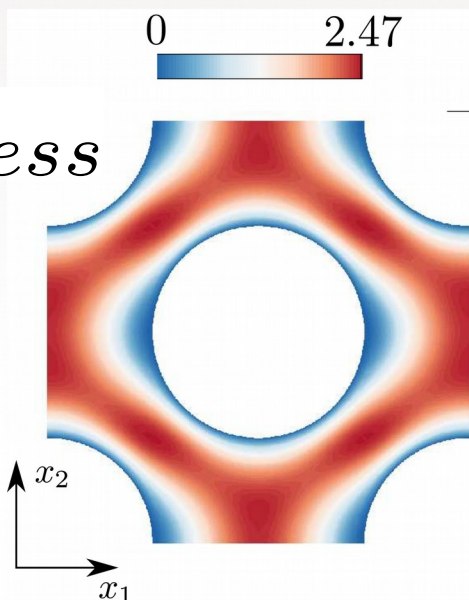
DNS: $\varepsilon = 0.6$

$Re_d = 0$

$Re_d = 10$

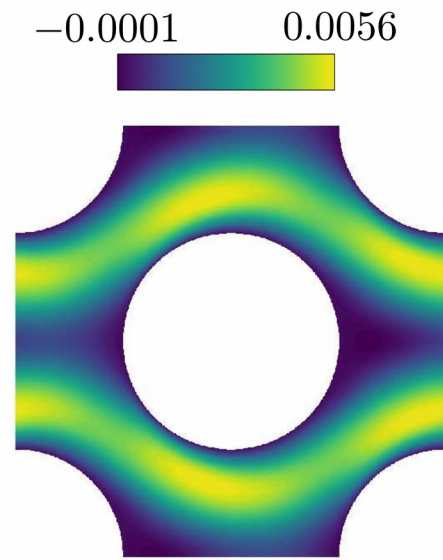
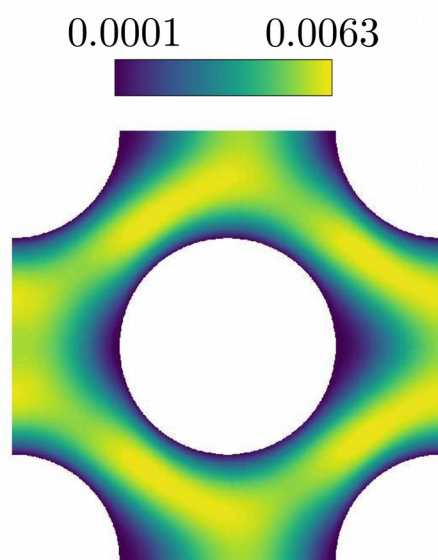
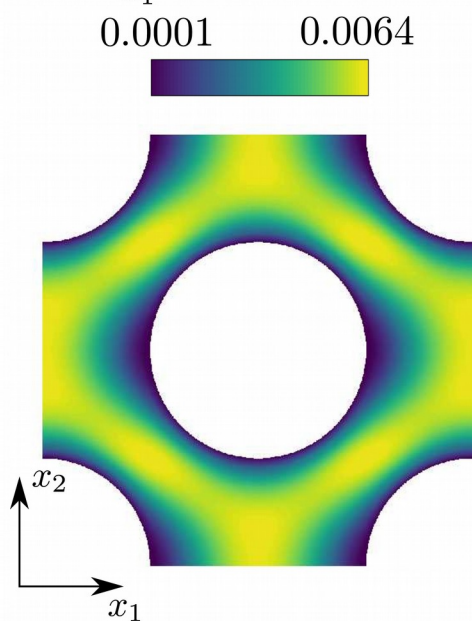
$Re_d = 50$

$U_{dimless}$



$$Re_e = \frac{d \langle U \rangle^i}{\nu_\beta}$$

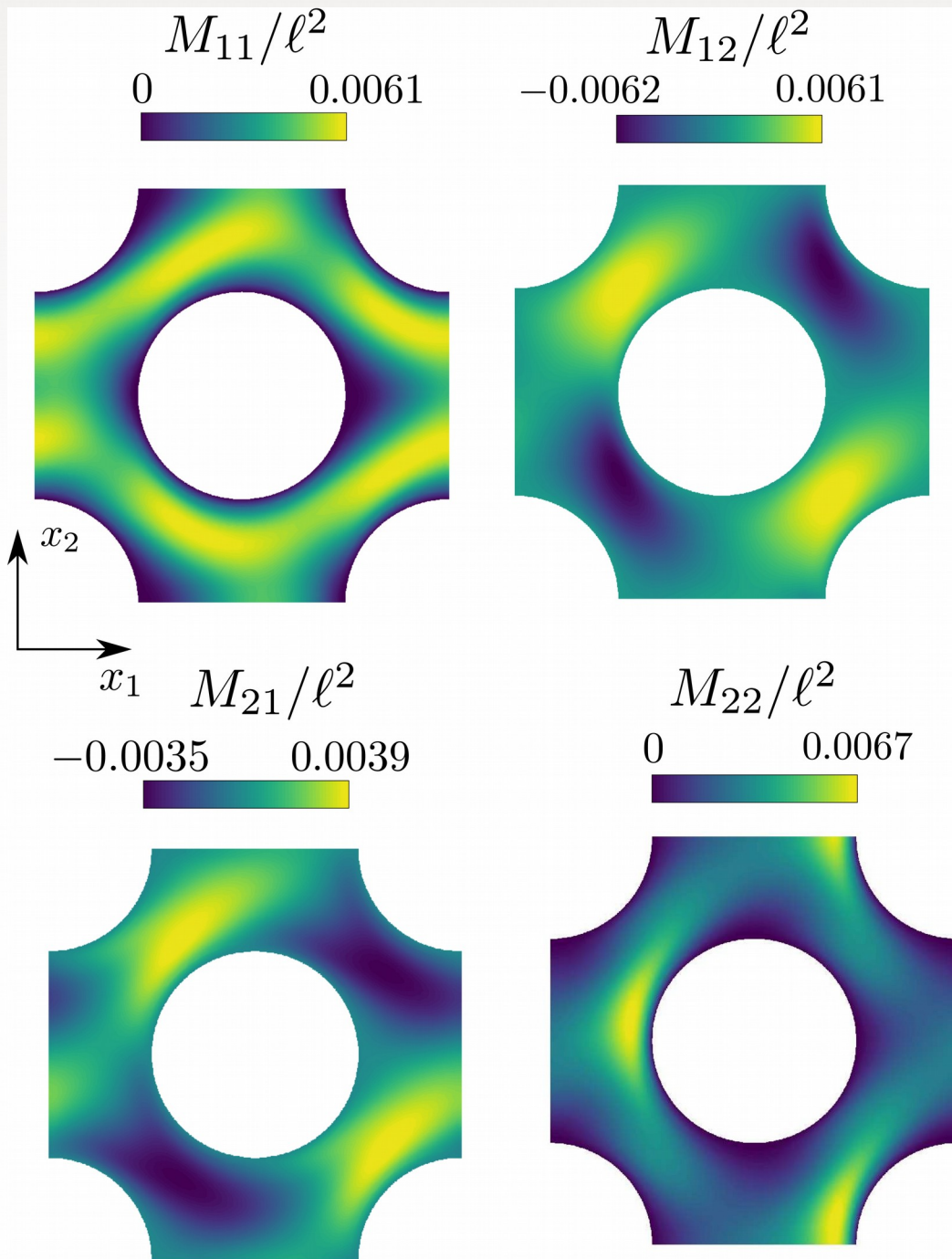
M_{11}



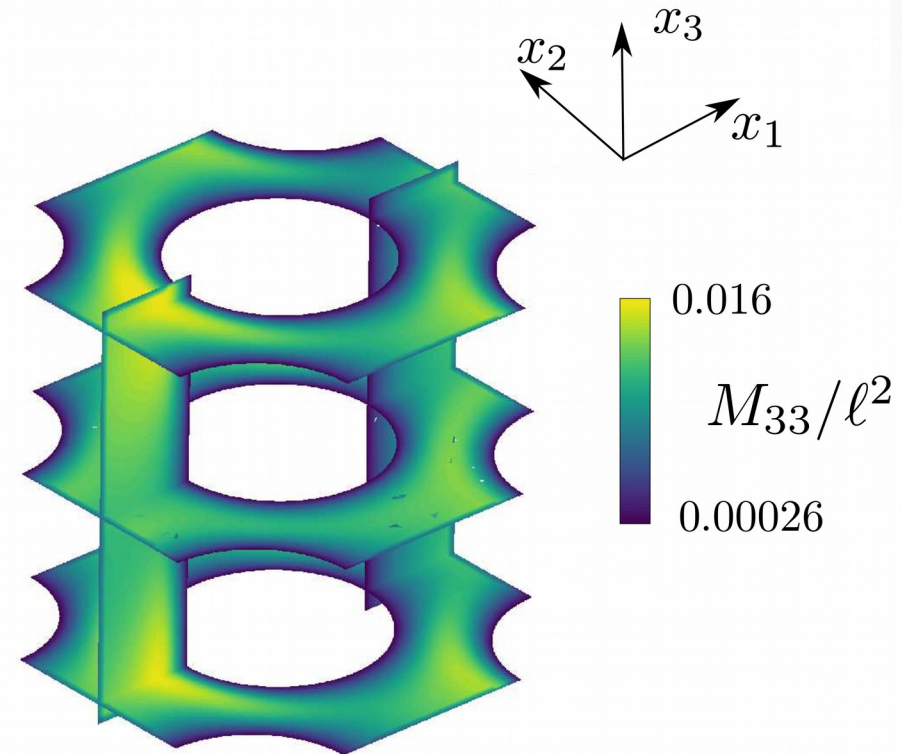
M FIELDS:

$$\theta = 22.5^\circ, \quad \varphi = 45^\circ,$$

$$\text{Re}_d = 50, \quad \varepsilon = 0.6$$

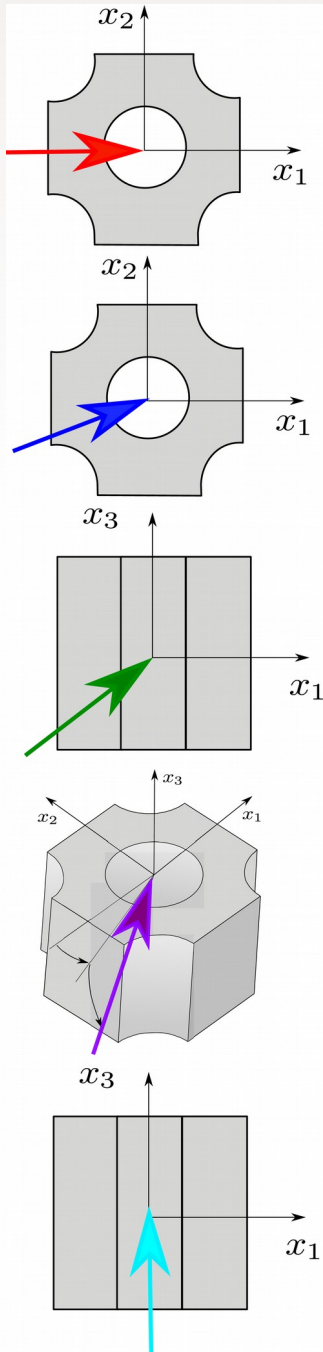


Non-diagonal fields not null
11-22 fields of same order of magnitude



33 fields are almost twice as large as 11

PARAMETERS EXPLORATION



index	θ	ϕ	field properties
1	0°	0°	2D symmetric
2	22.5°	0°	2D non-symmetric
3	0°	45°	3D symmetric
4	22.5°	45°	3D non-symmetric
5	—	90°	3D symmetric

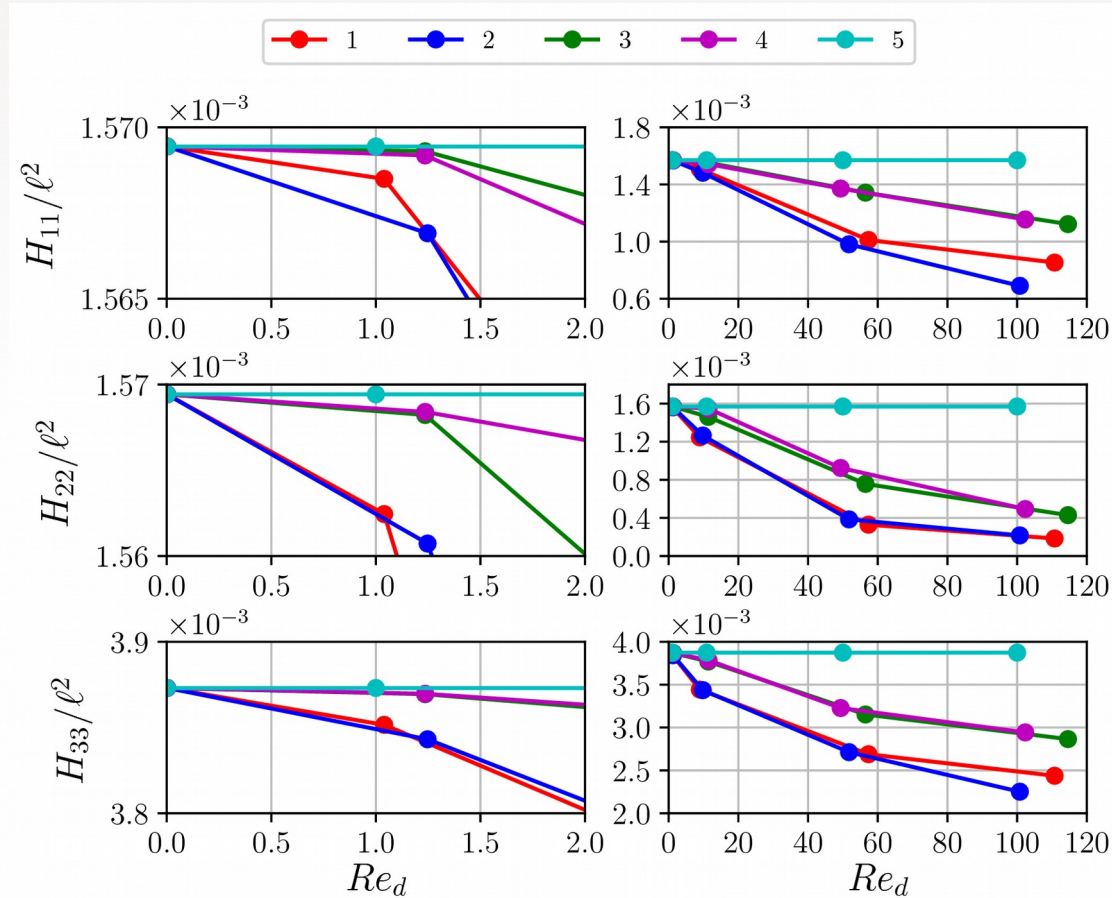
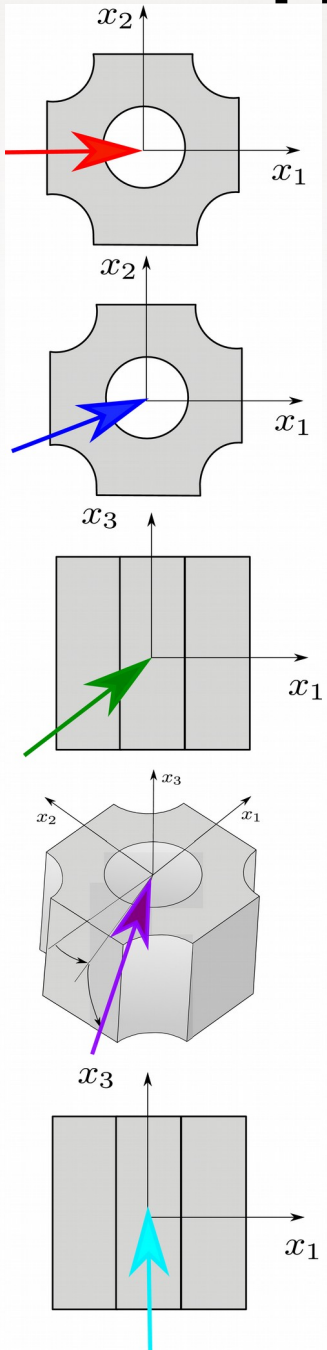
For each of the 5 directions the computation of H is carried out.

The variability of 3 values of porosity 0.4, 0.6, 0.8 are explored

Reynolds number is also changed



H COMPONENTS FOR $\varepsilon = 0.6$

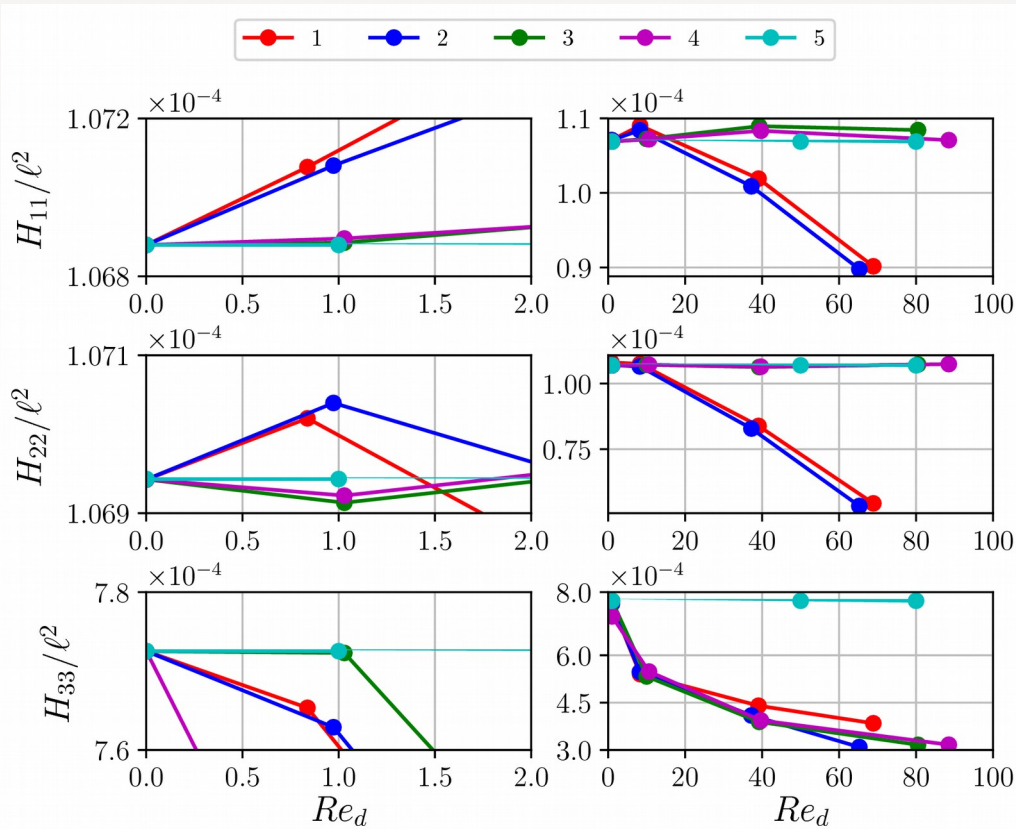


At small Reynolds number the variability is very small

At “high” Reynolds number is possible to distinguish between directions especially with the angle Φ

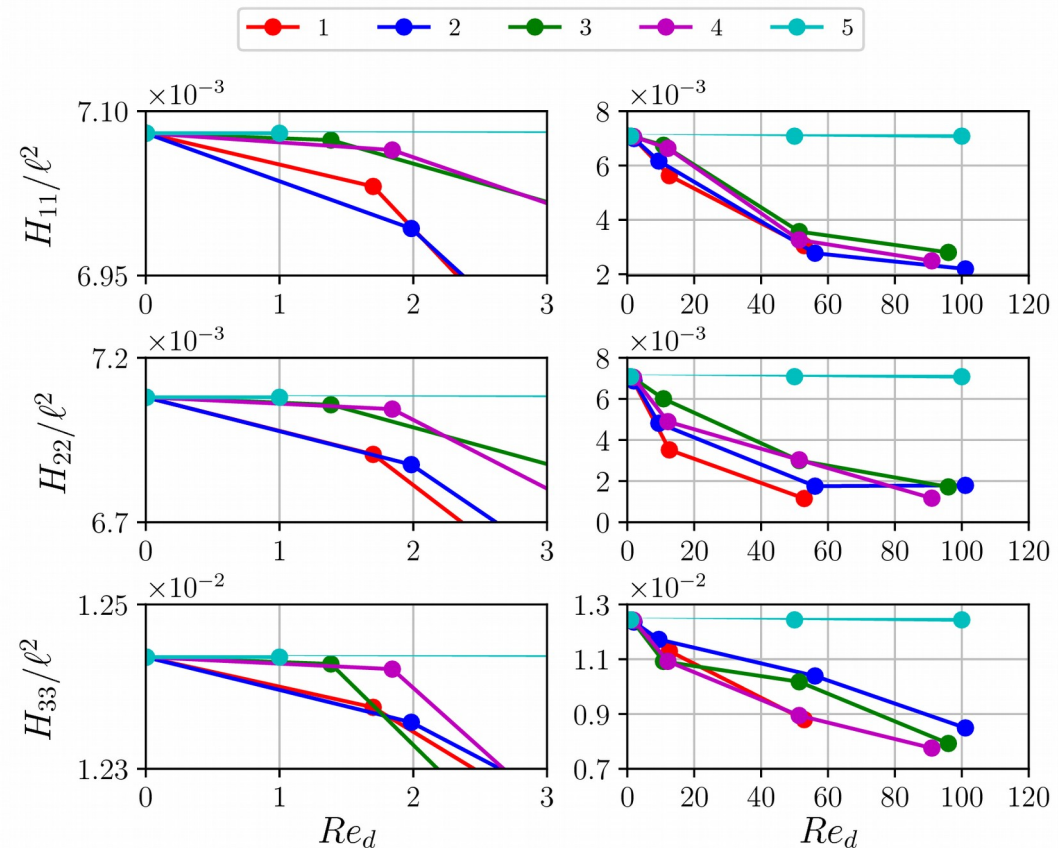


H COMPONENTS FOR $\varepsilon = 0.4, 0.8$

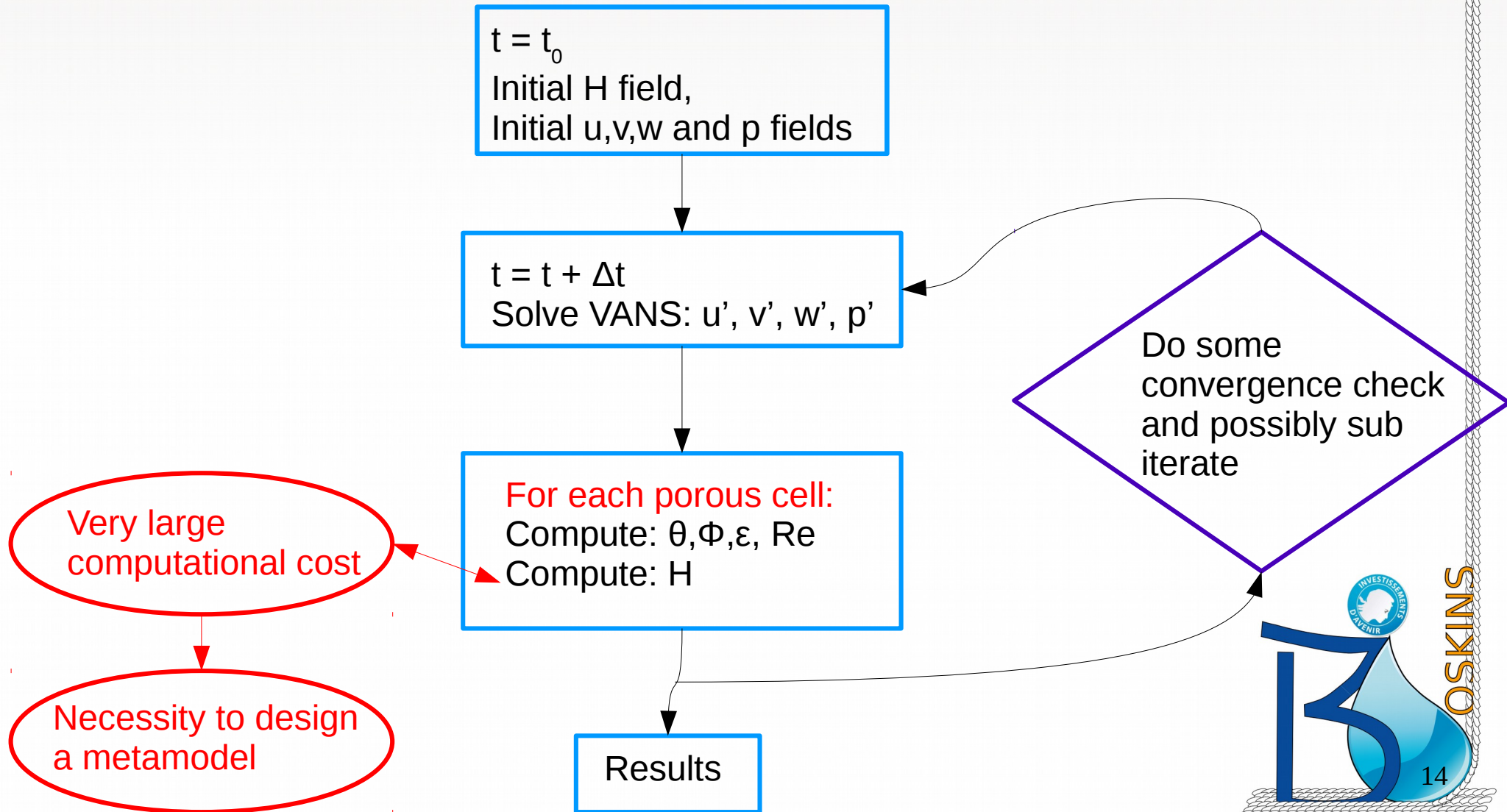


At low porosity ($\varepsilon = 0.8$, on the right) the curves almost collapse onto one another except for the case with the velocity aligned with the fibre's axis

At low porosity ($\varepsilon = 0.4$, on the left) the variability is smaller than before and as before the angle Φ seems to play a bigger role



MACROSCOPIC SIMULATION ALGORITHM:



DACE: DESIGN AND ANALYSIS OF COMPUTER EXPERIMENTS

“an experiment is a series of tests in which the input variables are **changed according to a given rule** in order to identify the reasons for the changes in the output response”[1]

The choice of the “rule” depends on:

- Number of variables (parameters)
- Number of feasible “experimental” runs: N
- Nature of variables (discrete vs continuous)
- Outputs of the experiment



DACE ANALYSIS

Random Monte Carlo

- Building response surfaces
- N is a user choice

A jungle of models can be used:

- Tagushi tables
- Full factorial design
- Latin hypercube
- Chebichev polynomials
- ...

parameter	values				
θ	0°	22.5°	45°		
ϕ	0°	22.5°	45°	67.5°	90°
Re_d	0	10	50	100	
ε	0.4	0.6	0.8		

Total numbers of experiments : 118

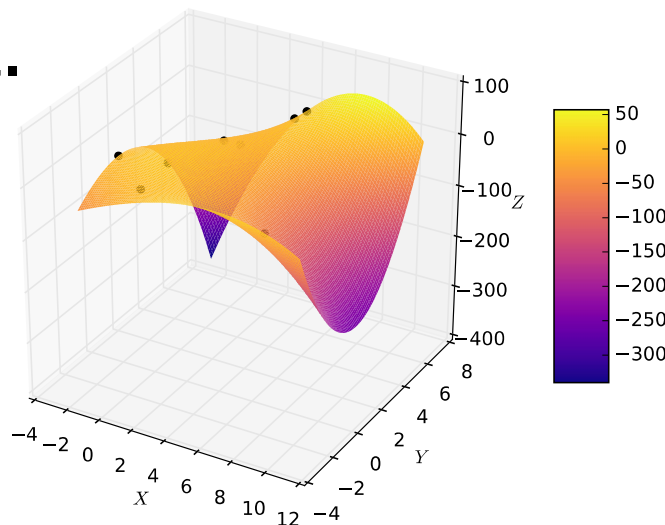


WHAT IS A METAMODEL?

- “A metamodel is a model of a model...” from wikipedia

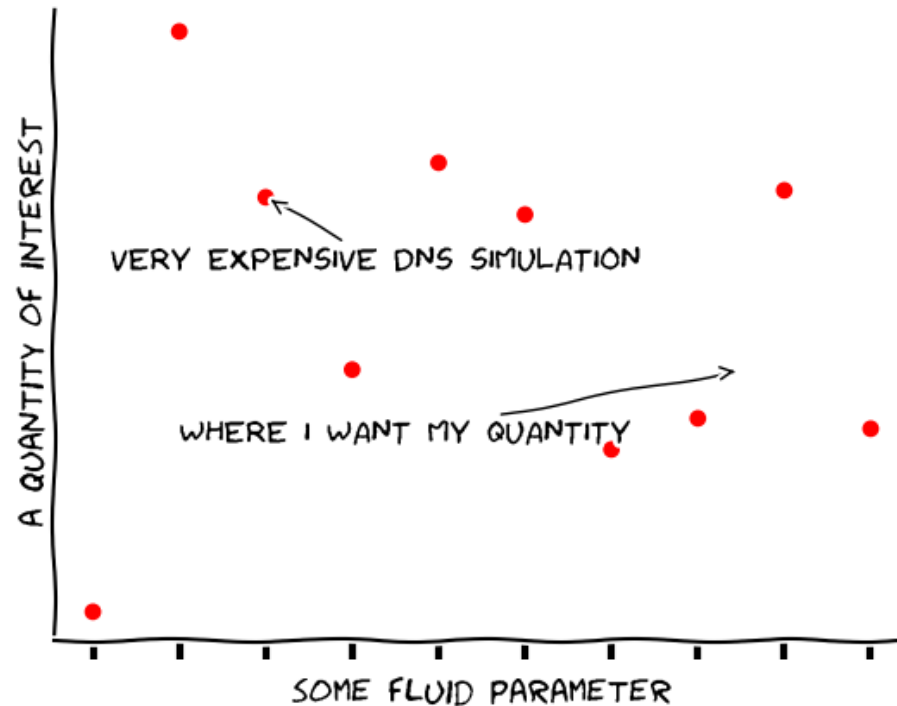


- It is a simpler/cheaper way (simpler than the parent model) to generate new output values of an experiment.



WHEN DO WE NEED IT ?

- Whenever your parent model is too “heavy”
- If you do not know the parent model (machine learning)

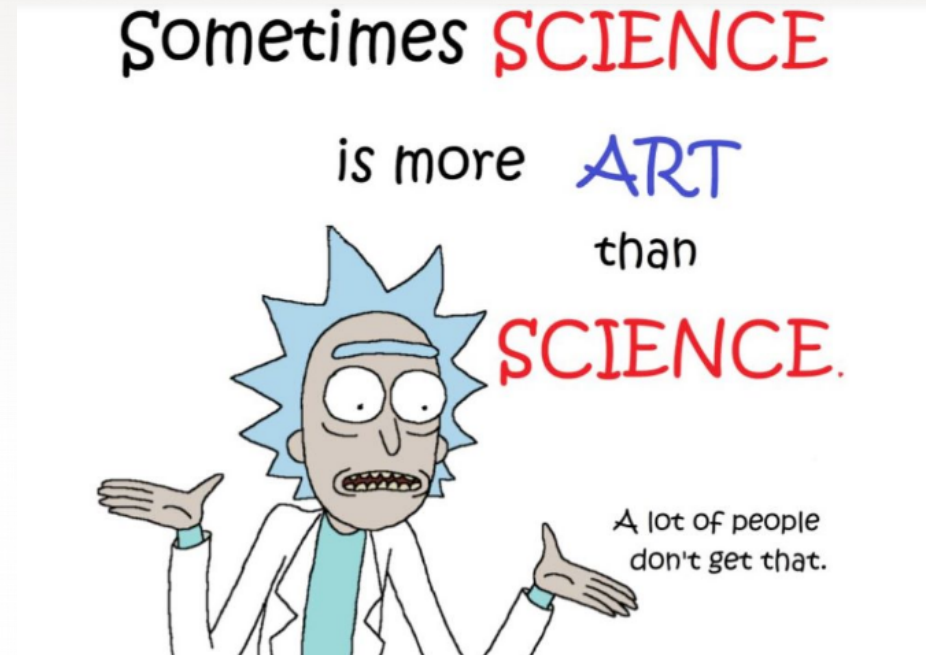


- Example: Optimization, Uncertainty Quantification, Flow Control



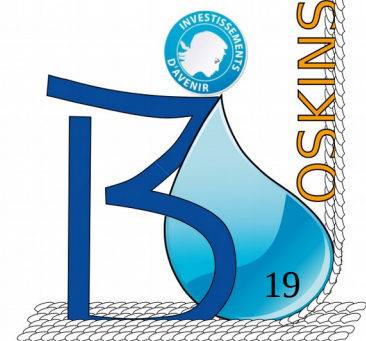
WHICH MODEL IS "THE BEST" ?

- Number of data points
- Distributions of data points
- Availability as library / easyness of implementation
- Domain of applications
- Minimize errors
- Number of variables
- Noise presence, interpolation vs approximation



There is a really jungle of possibilities:

- Least Square regression
- P-th polynomial
- Polynomial chaos
- Radial basis functions
- Deep learning



KRIGING METAMODEL

- The **predictor** is a sum of a **trend function** and a **Gaussian process** error model

$$y(\mathbf{x}) \approx \hat{f}(\mathbf{x}) = t(\mathbf{x}) + e(\mathbf{x})$$

Quadratic
Least Square

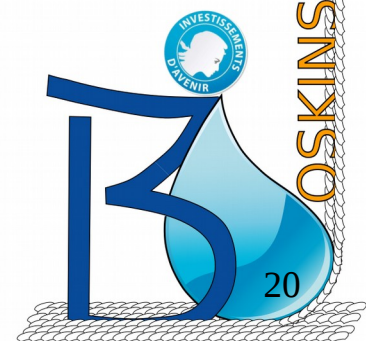
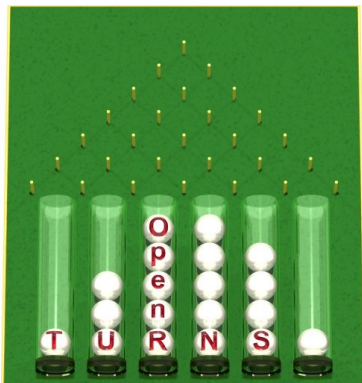
Gaussian process

$$\text{Cov}(y(\mathbf{x}_i), y(\mathbf{x}_j)) = \sigma^2 r(\mathbf{x}_i, \mathbf{x}_j)$$

$(\theta, \phi, Re_d, \varepsilon)$

(H_{11}, H_{22}, H_{33})

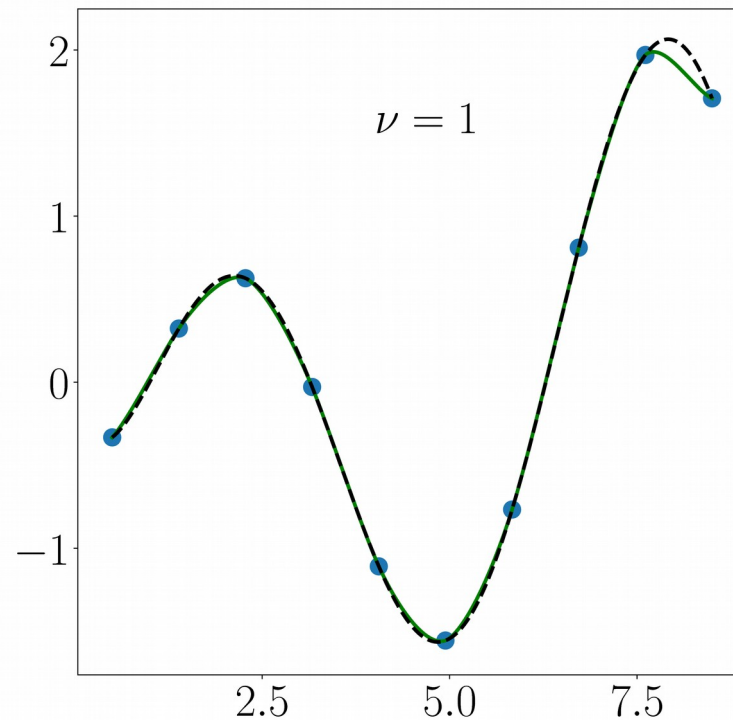
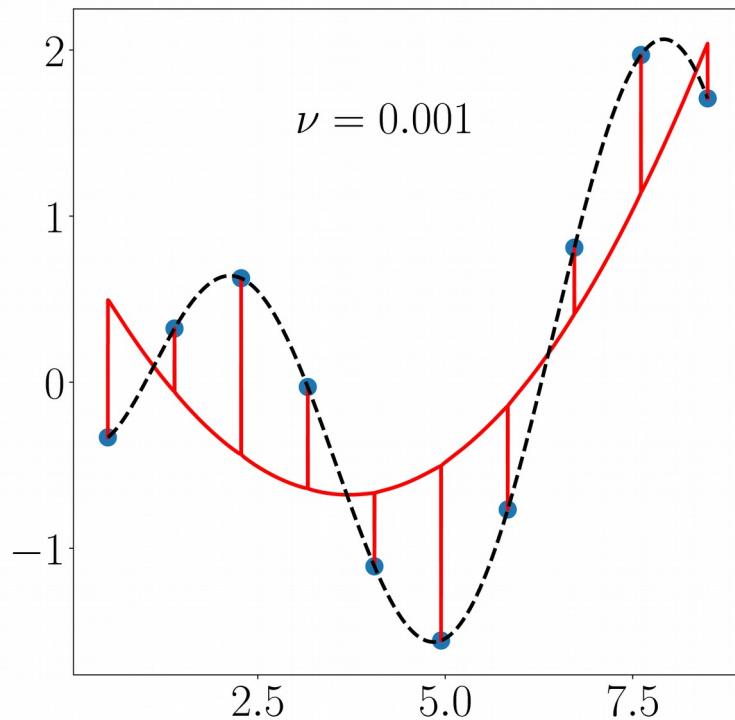
$(\mathbf{x}_i, y(\mathbf{x}_i))$



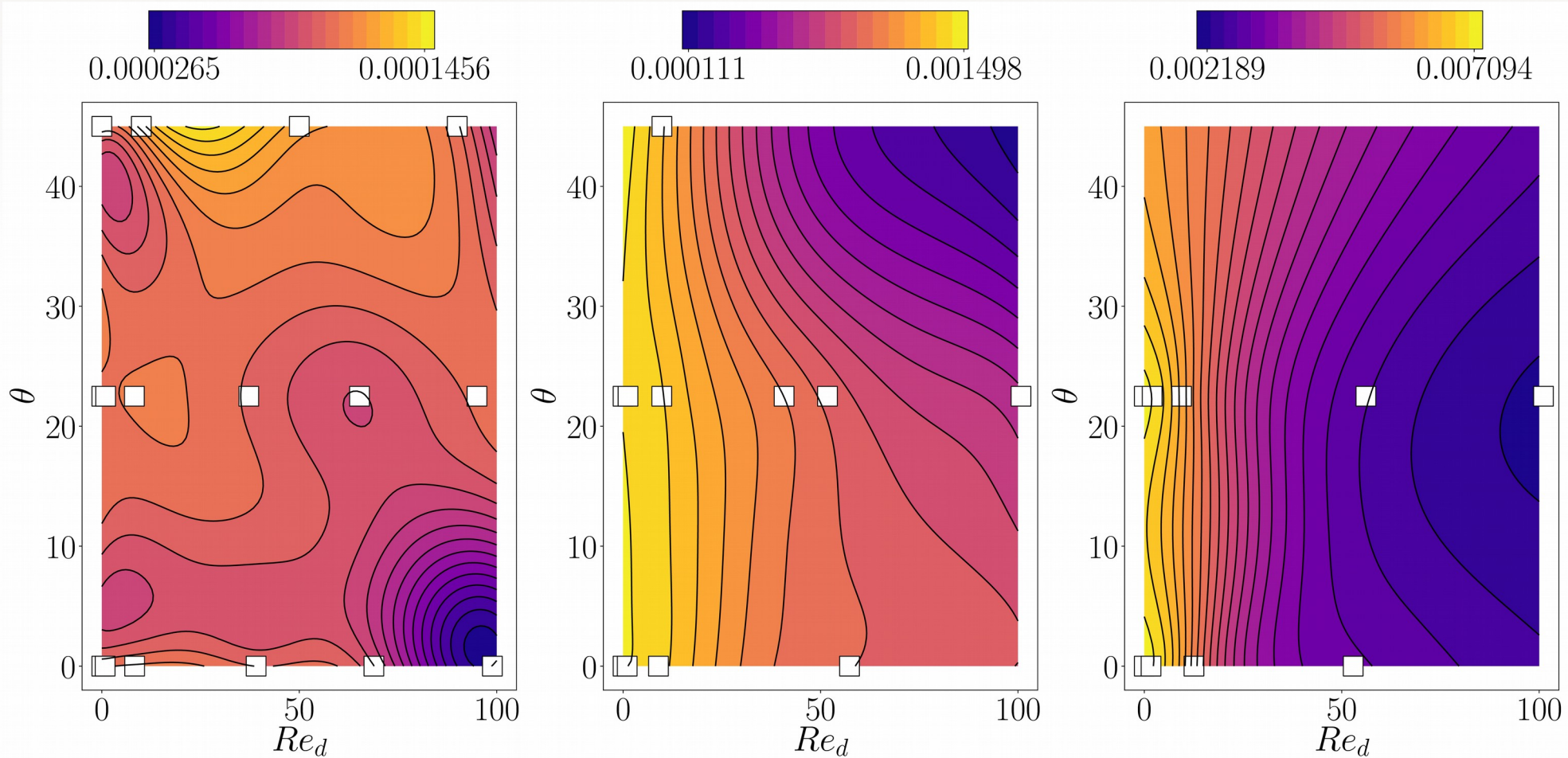
COVARIANCE MODEL

Matérn covariance model:

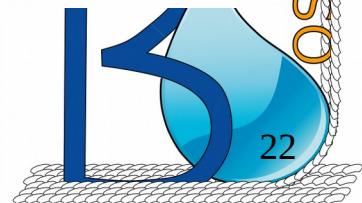
$$r(\mathbf{x}_i, \mathbf{x}_j) = \frac{2^{1-\nu}}{\Gamma(\nu)} \left(\frac{\sqrt{2\nu}|\mathbf{x}_i - \mathbf{x}_j|}{|\lambda|} \right)^\nu K_\nu \left(\frac{\sqrt{2\nu}|\mathbf{x}_i - \mathbf{x}_j|}{|\lambda|} \right)$$



RESULTS: H_{\parallel} WITH $\varphi = 0^\circ$ AND $\varepsilon = 0.4, 0.6, 0.8$



Variation of the apparent permeability with the angle θ is weak

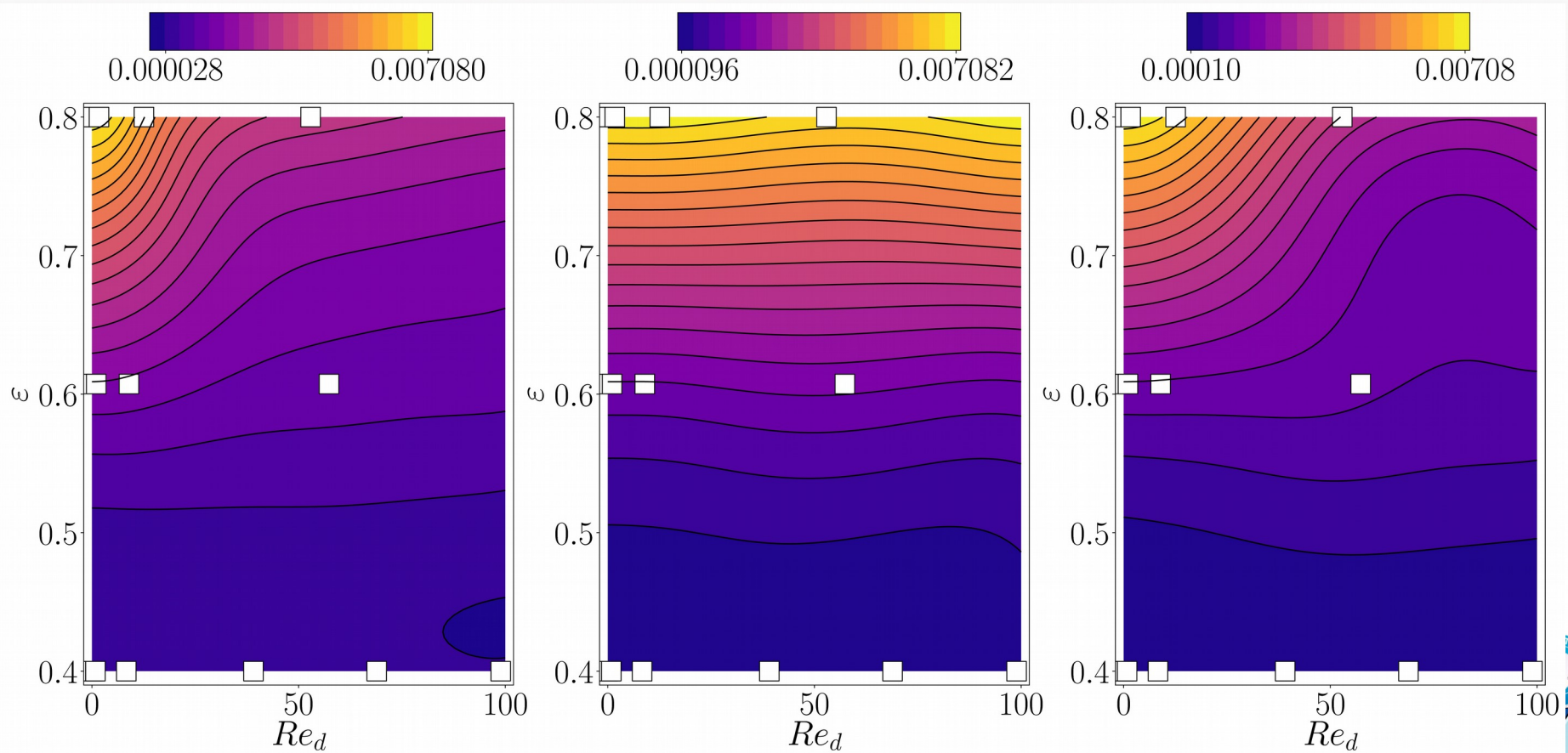


RESULTS: H_{11}

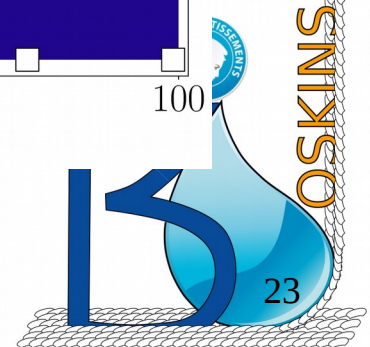
$$\phi = \theta = 0^\circ$$

$$\phi = 90^\circ$$
$$\theta = 0^\circ$$

$$\phi = 45^\circ$$
$$\theta = 22.5^\circ$$



The apparent permeability can change by one order of magnitude in the range of the analysed porosity



CONCLUSION AND FUTURE WORK:

NAVIER-STOKES

VANS AVERAGING

CLOSURE PROBLEMS

DACE

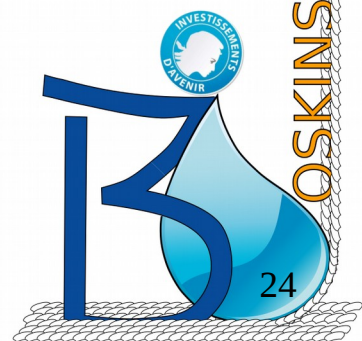
KRIGING METAMODEL

MACRO MODEL NS + POROUS

- The work presented has been submitted to “Computer and Fluids”
- We have shown that the tensor H can vary with the fluid flow
- Kriging metamodeling can be a good choice to update H at each time iteration in a NS+porous solver

Next steps:

- Integrate the Kriging metamodel inside the OpenFOAM solver



DACE JUNGLE

Full Factorial:

- Computing the main and the interaction effects
- Building response surfaces
- N is fixed

Taguchi:

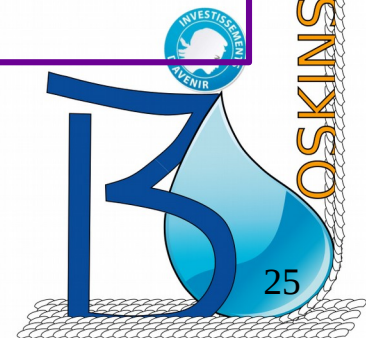
- Addressing the influence of noise variables
- N is fixed

Latin hypercube:

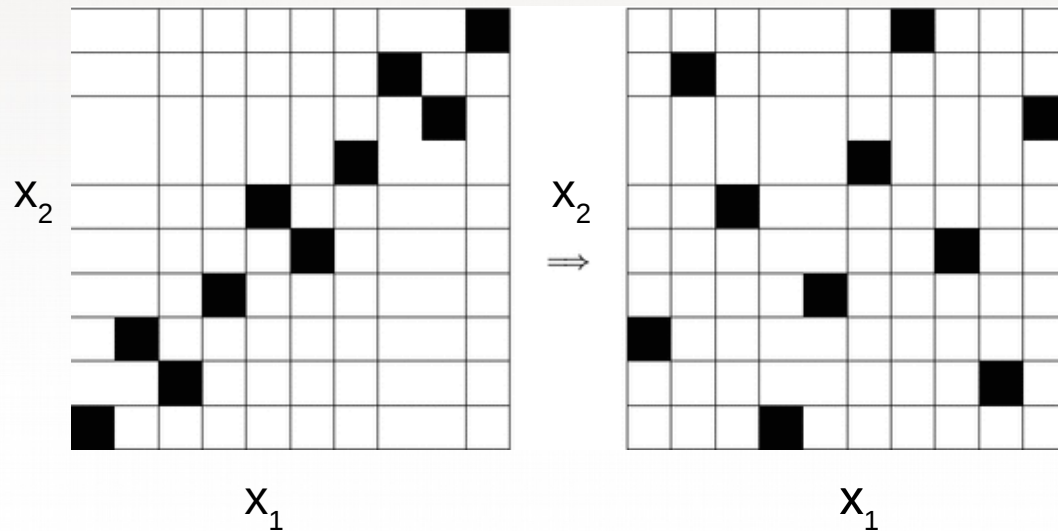
- Building response surfaces
- N is a user choice

Random Monte Carlo

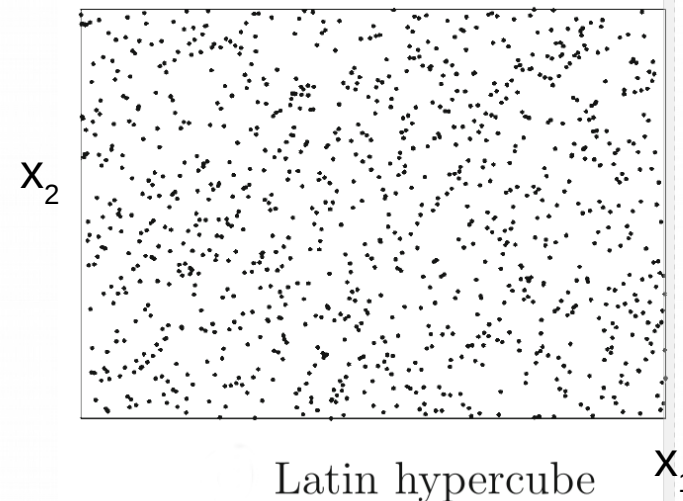
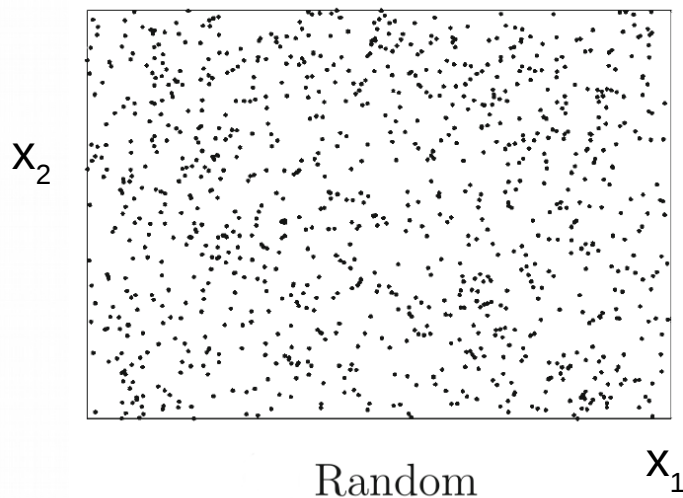
- Building response surfaces
- N is a user choice



DACE VARIABILITY



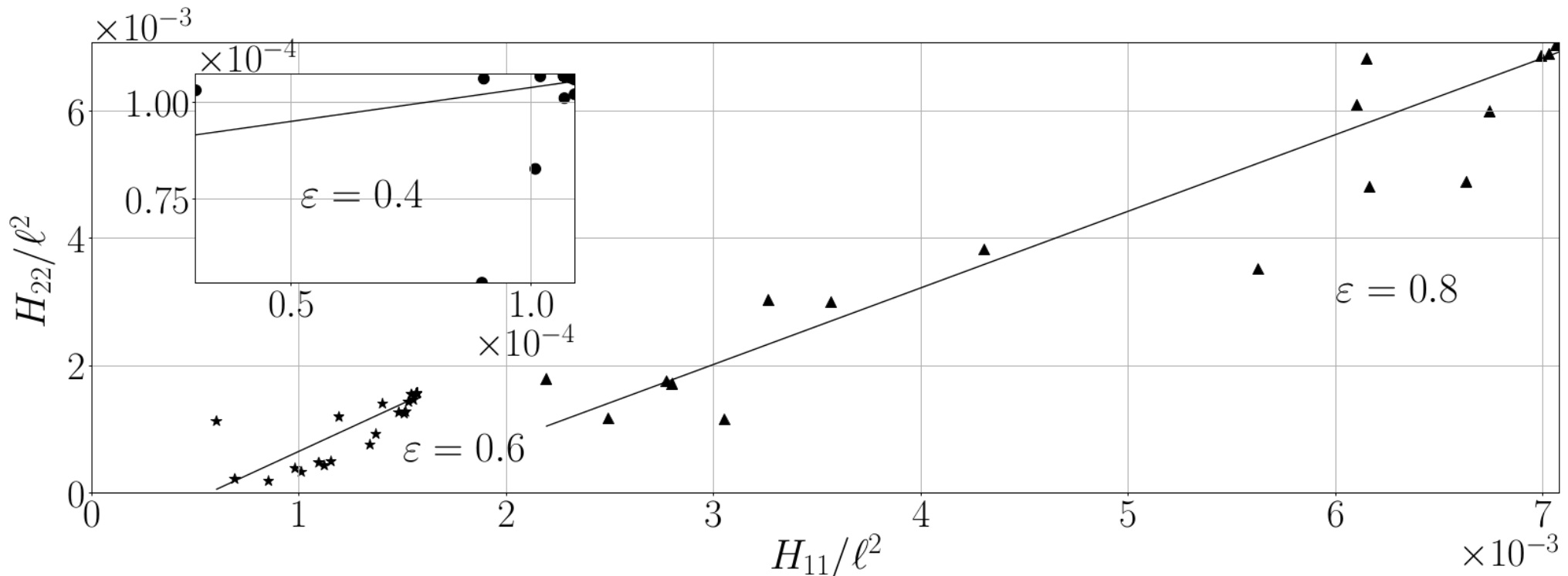
- LH should be carefully designed but it is often the best choice when we cannot afford large N
- With higher N the results tend to be similar



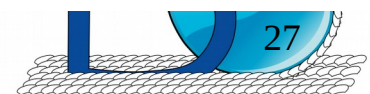
DATA ANALYSIS

parameter	values				
θ	0°	22.5°	45°		
ϕ	0°	22.5°	45°	67.5°	90°
Re_d	0	10	50	100	
ε	0.4	0.6	0.8		

Total numbers of experiments : 118

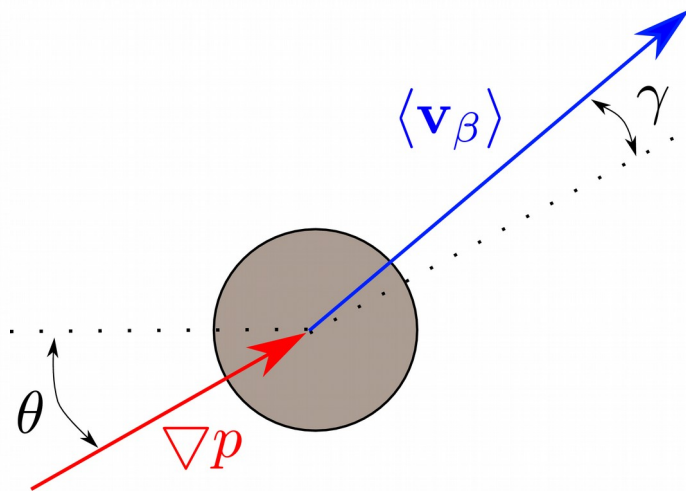


Correlations appear among the elements of the permeability tensor



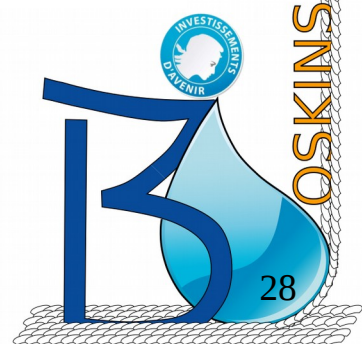
FORCING AND VELOCITY ANGLES CORRELATION

$$(u_\beta, v_\beta, w_\beta) \sim \left(H_{11} \frac{\partial p}{\partial x_1}, H_{22} \frac{\partial p}{\partial x_2}, H_{33} \frac{\partial p}{\partial x_3} \right)$$

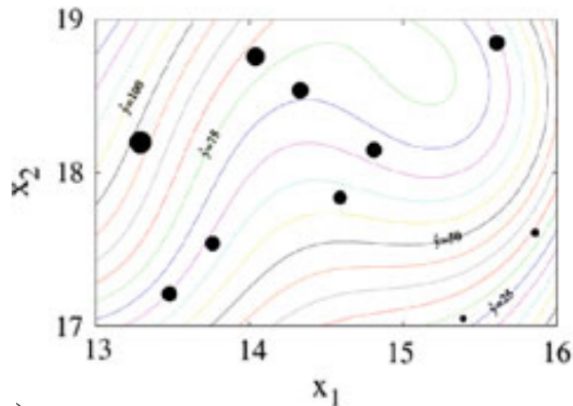


$$\tan \gamma = \frac{\left(1 - \frac{H_{11}}{H_{22}} \right) \tan \theta}{\frac{H_{11}}{H_{22}} + \tan^2 \theta}$$

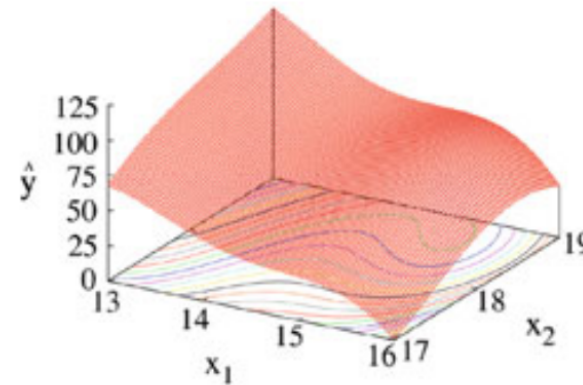
Deviation angles are connected to the permeability tensor



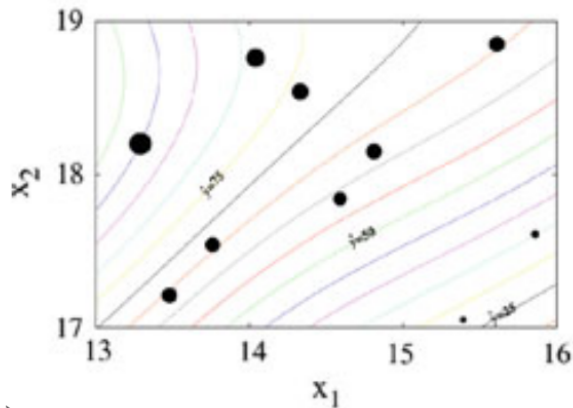
KRIGING VARIABILITY EXAMPLES



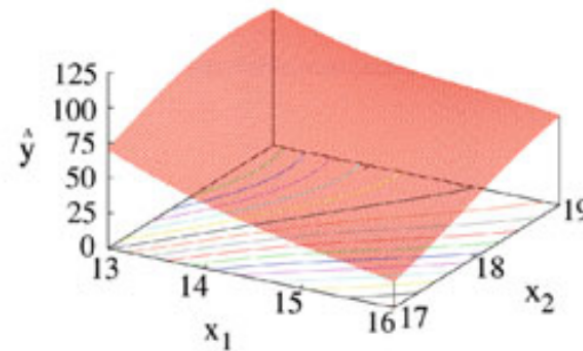
(a) Gaussian model, $C_0 = 0$, $C_1 = 1478$, $R = 2.68$, $\frac{C_0}{C_1} = 0$, $R_{pr} = 4.66$, contour view



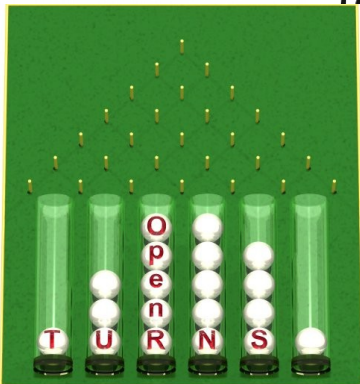
(b) Gaussian model, $C_0 = 0$, $C_1 = 1478$, $R = 2.68$, $\frac{C_0}{C_1} = 0$, $R_{pr} = 4.66$, 3d view



(c) Gaussian model, $C_0 = 7.39$, $C_1 = 1478$, $R = 2.68$, $\frac{C_0}{C_1} = 0$, $R_{pr} = 4.66$, contour view

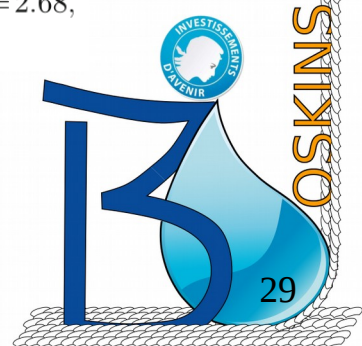


(d) Gaussian model, $C_0 = 7.39$, $C_1 = 1478$, $R = 2.68$, $\frac{C_0}{C_1} = 0$, $R_{pr} = 4.66$, 3d view

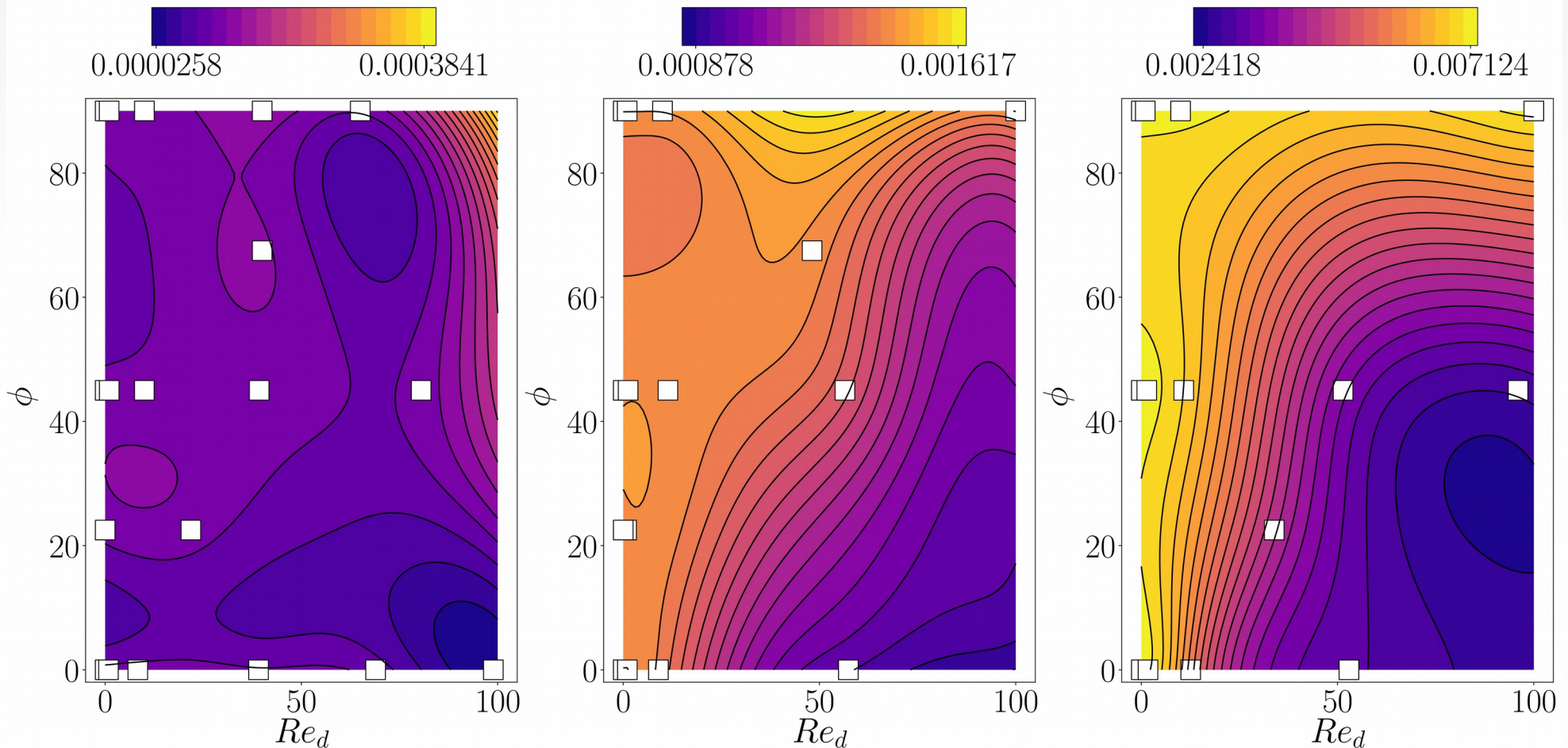


There are a lot of parameters to play with and they can change a lot your model

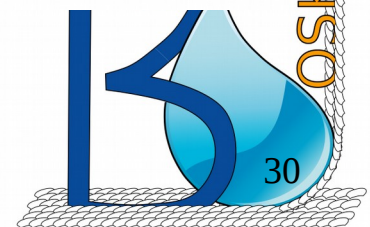
Image from "Optimization Methods", Marco Cavazzuti, Springer 2012



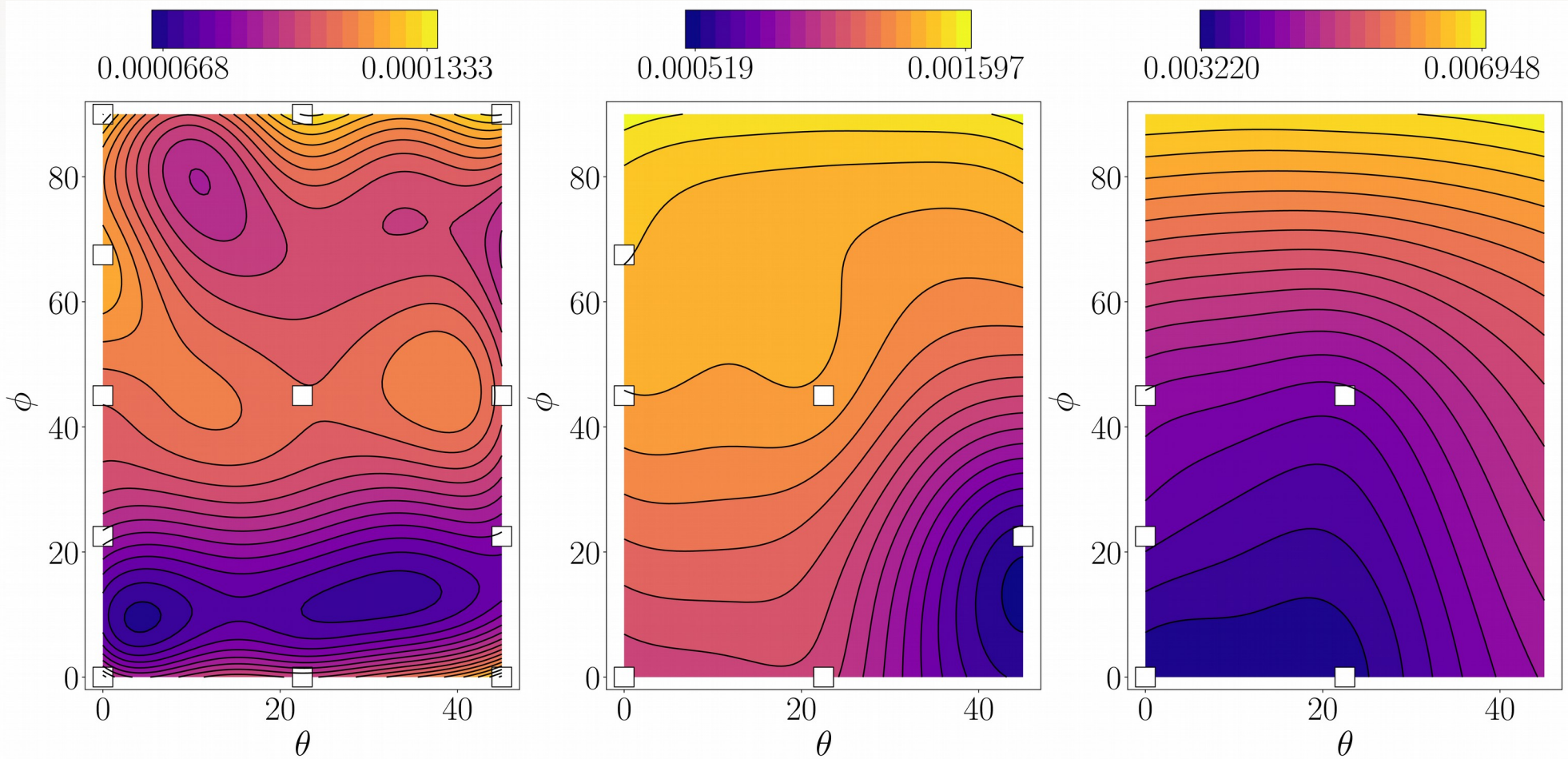
RESULTS: H_{11} WITH $\theta = 0^\circ$ AND $\varepsilon = 0.4, 0.6, 0.8$



Variations with respect to ϕ are more pronounced than those found with respect to θ and are due to a real three-dimensionalization of the flow



RESULTS: H_{11} WITH RE = 40 AND $\varepsilon = 0.4, 0.6, 0.8$



H_{11} has a much stronger dependence on ϕ than on θ , suggesting that the real test of permeability models must include three-dimensional effects

