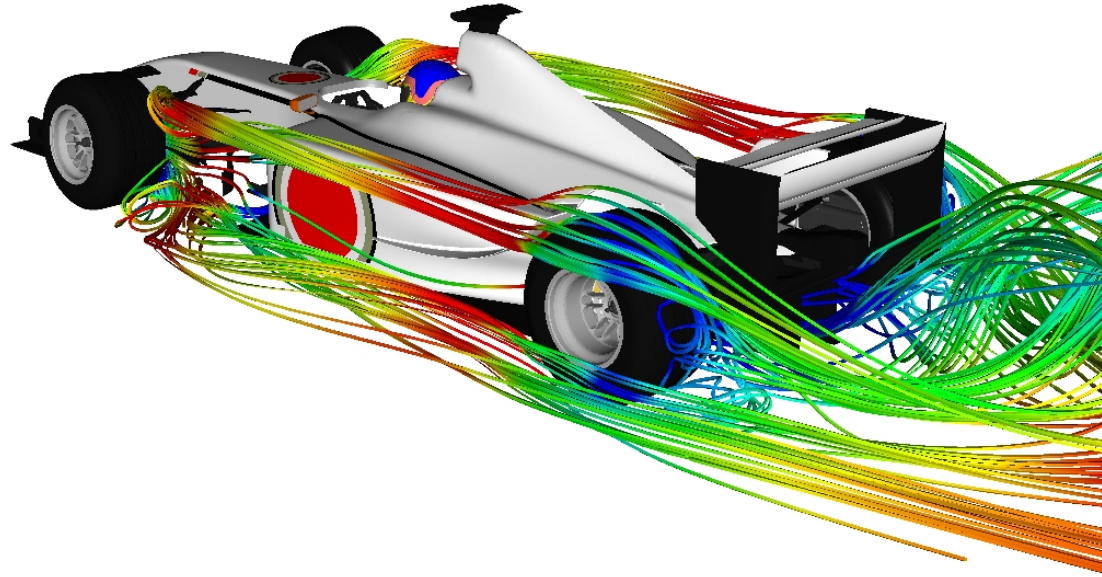
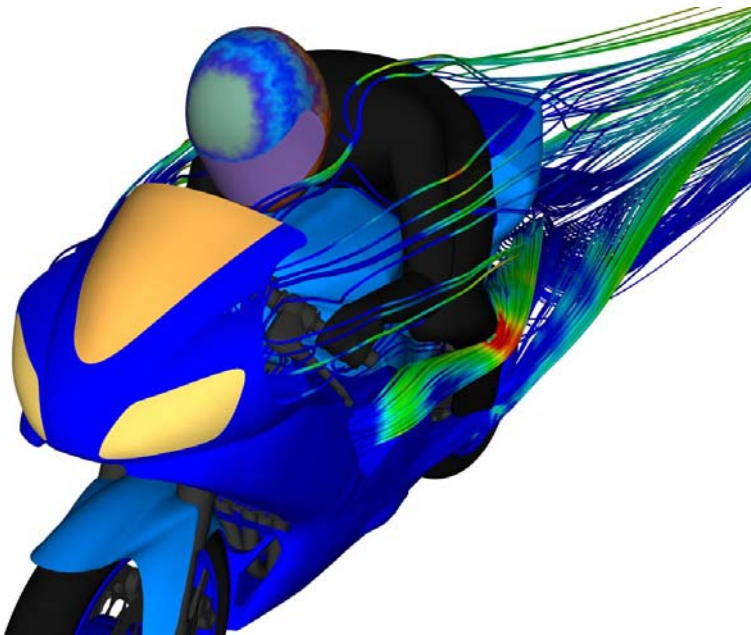


# Chapter 11: Flow over bodies. Lift and drag

# Objectives

- Have an intuitive understanding of the various physical phenomena such as drag, friction and pressure drag, drag reduction, and lift.
- Calculate the drag force associated with flow over common geometries.
- Understand the effects of flow regime on the drag coefficients associated with flow over cylinders and spheres
- Understand the fundamentals of flow over airfoils, and calculate the drag and lift forces acting on airfoils.

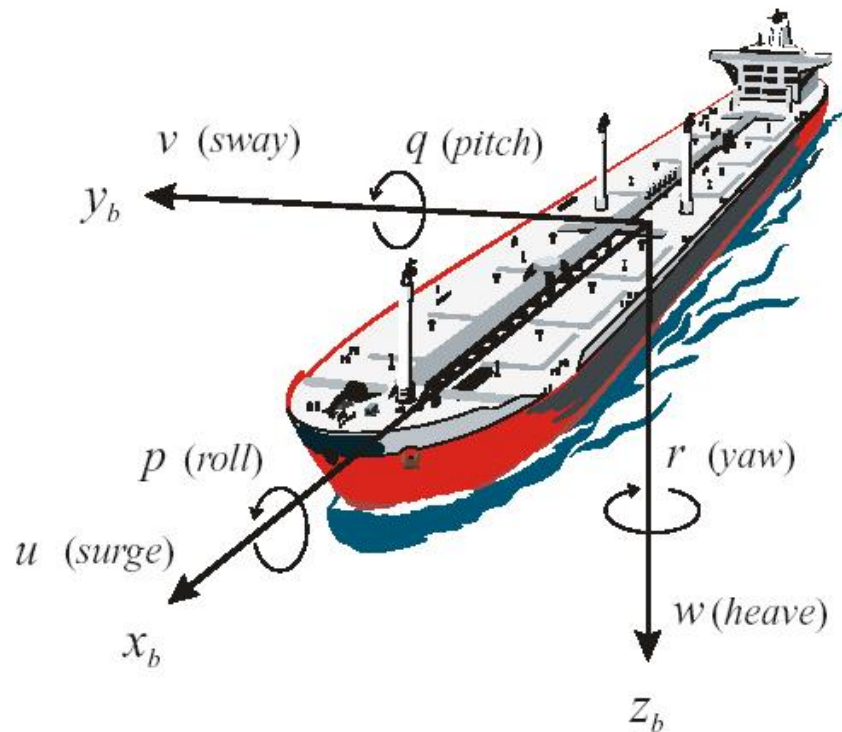
# Motivation



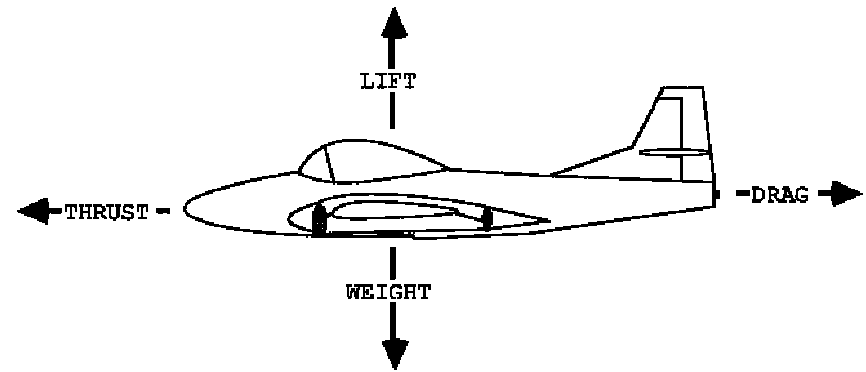
# External Flow

- Bodies and vehicles in motion, or with flow over them, experience fluid-dynamic forces and moments.
- Examples include: aircraft, automobiles, buildings, ships, submarines, turbomachines.
- These problems are often classified as ***External Flows***.
- Fuel economy, speed, acceleration, maneuverability, stability, and control are directly related to the aerodynamic/hydrodynamic forces and moments.
- General 6DOF motion of vehicles is described by 6 equations for the linear (surge, sway, heave) and angular (roll, pitch, yaw) momentum.

# Fluid Dynamic Forces and Moments

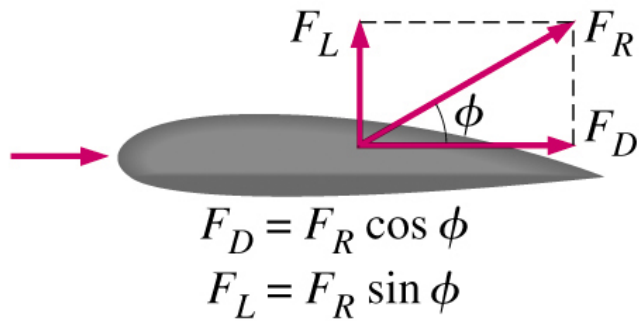


Ships in waves present one of the most difficult 6DOF problems.

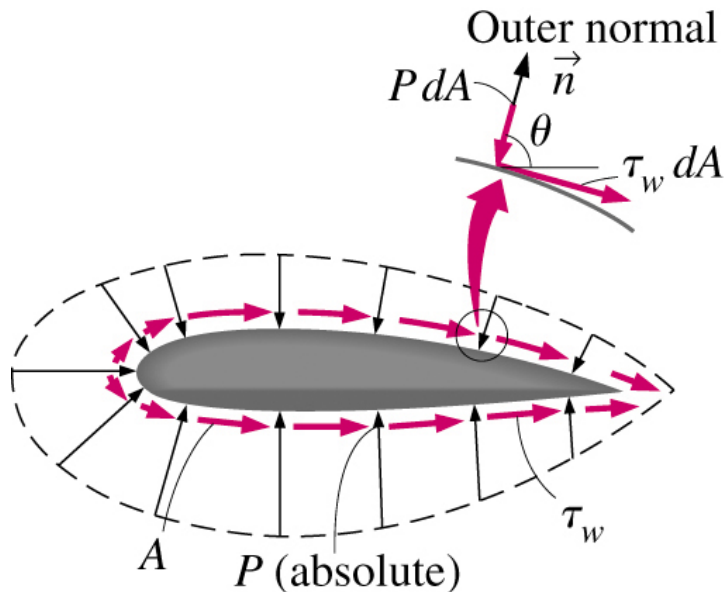


Airplane in level steady flight: drag = thrust and lift = weight.

# Drag and Lift



- Fluid dynamic forces are due to pressure and viscous forces acting on the body surface.
- Drag: component parallel to flow direction.
- Lift: component normal to flow direction.

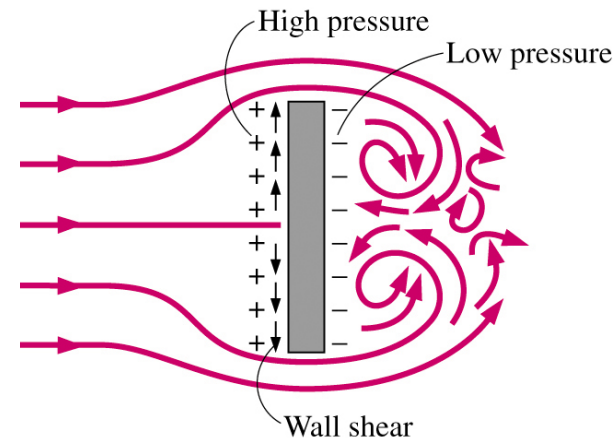
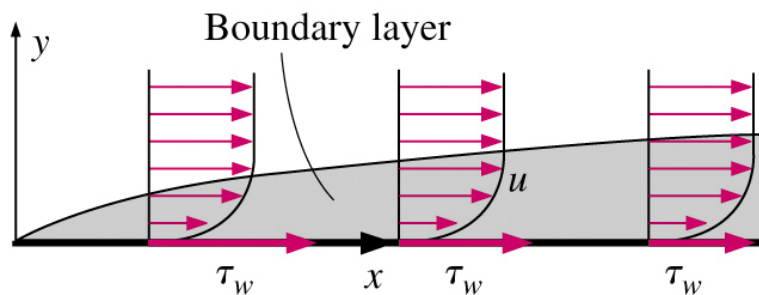


# Drag and Lift

- Lift and drag forces can be found by integrating pressure and wall-shear stress.

$$F_D = \int_A dF_D = \int_A (-P \cos\theta + \tau_w \sin\theta) dA$$

$$F_L = \int_A dF_L = - \int_A (P \sin\theta + \tau_w \cos\theta) dA$$



# Drag and Lift

- In addition to geometry, lift  $F_L$  and drag  $F_D$  forces are a function of density  $\rho$  and velocity  $V$ .
- Dimensional analysis gives 2 dimensionless parameters: lift and drag coefficients.

$$C_D = \frac{F_D}{\frac{1}{2}\rho V^2 A} \quad C_L = \frac{F_L}{\frac{1}{2}\rho V^2 A}$$

- Area  $A$  can be frontal area (drag applications), planform area (wing aerodynamics), or wetted-surface area (ship hydrodynamics).



# Example: Automobile Drag

Scion XB



Porsche 911



$$C_D = 1.0, A = 25 \text{ ft}^2, C_D A = 25 \text{ ft}^2$$

$$C_D = 0.28, A = 10 \text{ ft}^2, C_D A = 2.8 \text{ ft}^2$$

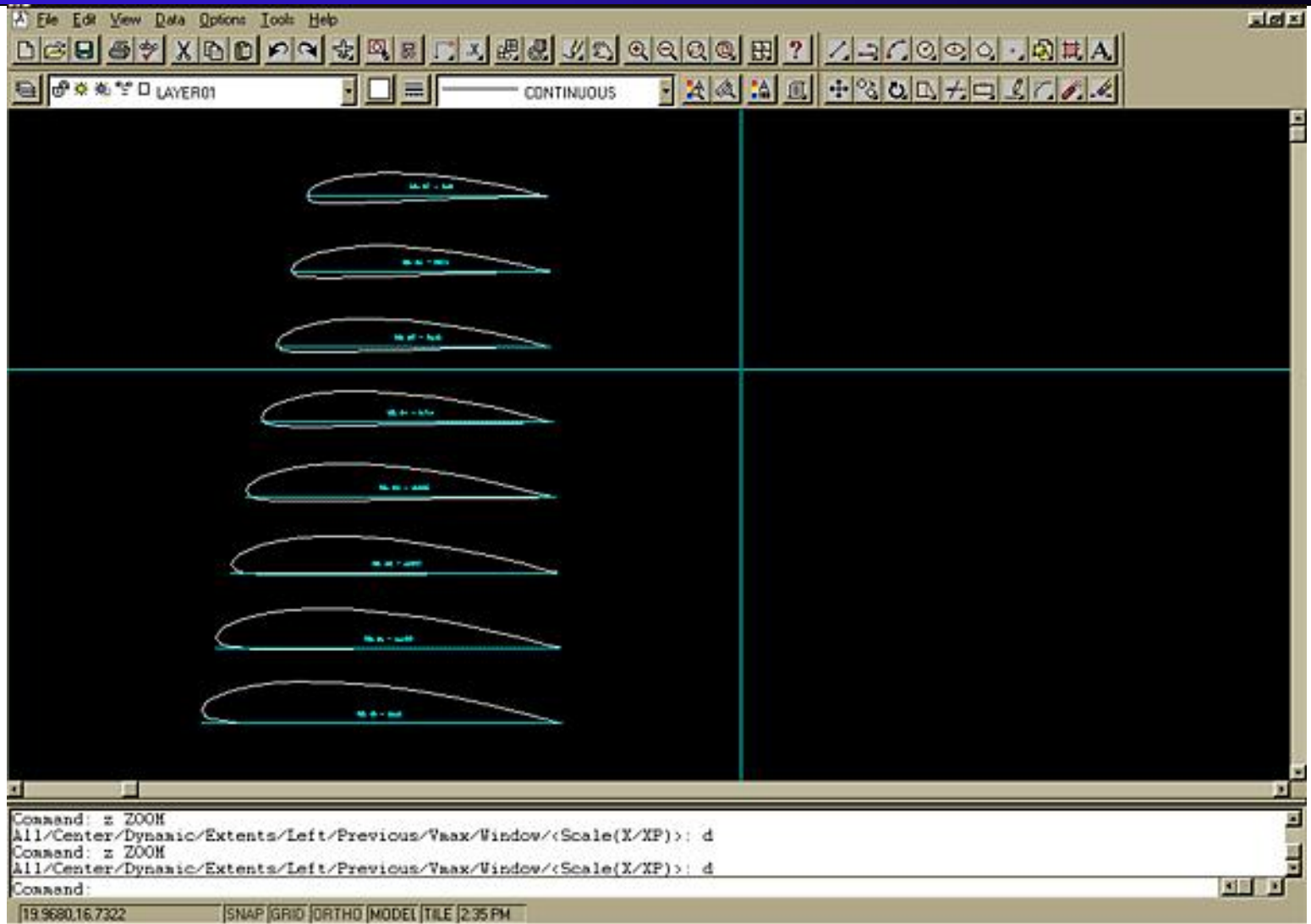
- Drag force  $F_D = 1/2 \rho V^2 (C_D A)$  will be  $\sim 10$  times larger for Scion XB
- Source is large  $C_D$  and large projected area
- Power consumption  $P = F_D V = 1/2 \rho V^3 (C_D A)$  for both scales with  $V^3$ !

# Drag and Lift

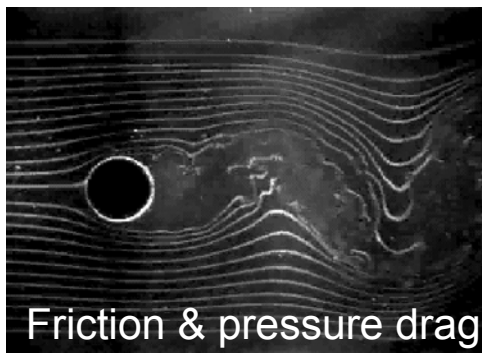
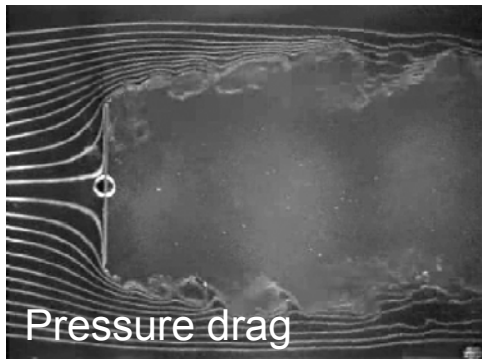
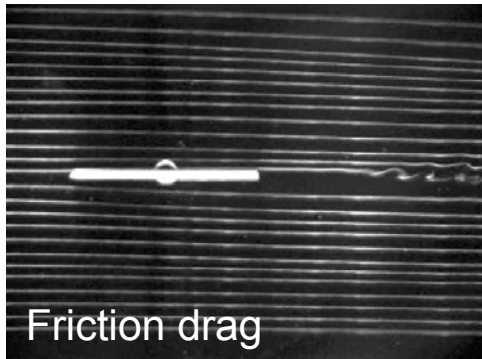
- For applications such as tapered wings,  $C_L$  and  $C_D$  may be a function of span location. For these applications, a local  $C_{L,x}$  and  $C_{D,x}$  are introduced and the total lift and drag is determined by integration over the span  $L$

$$C_L = \frac{1}{L} \int_0^L C_{L,x} dx \quad C_D = \frac{1}{L} \int_0^L C_{D,x} dx$$

# “Lofting” a Tapered Wing

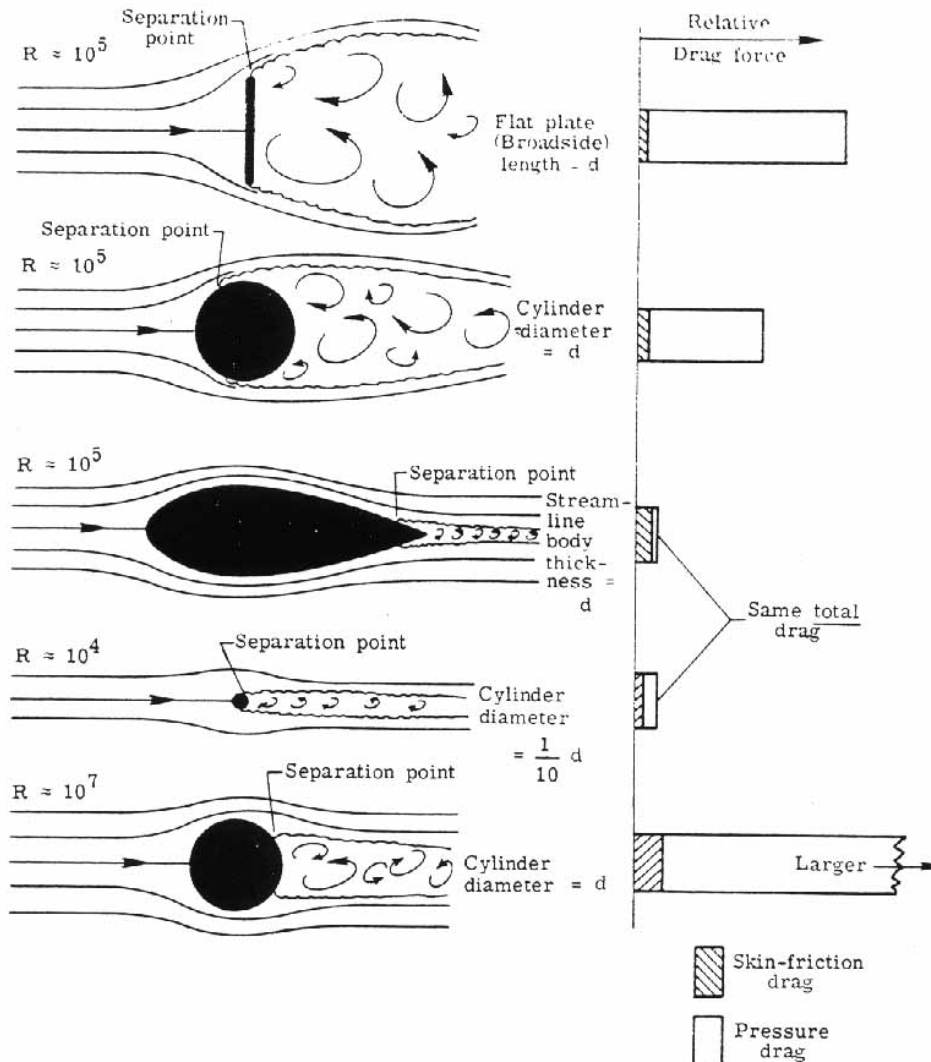


# Friction and Pressure Drag



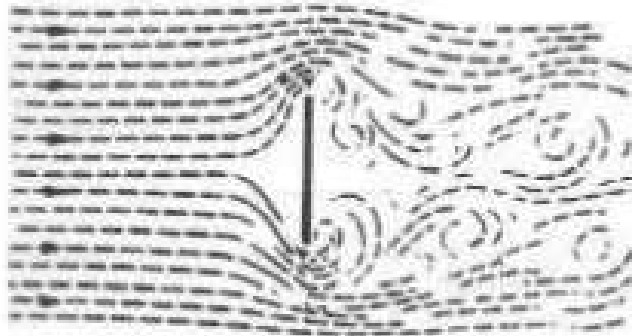
- Fluid dynamic forces are comprised of pressure and friction effects.
- Often useful to decompose,
  - $F_D = F_{D,friction} + F_{D,pressure}$
  - $C_D = C_{D,friction} + C_{D,pressure}$
- This forms the basis of ship model testing where it is assumed that
  - $C_{D,pressure} = f(Fr)$
  - $C_{D,friction} = f(Re)$

# Streamlining

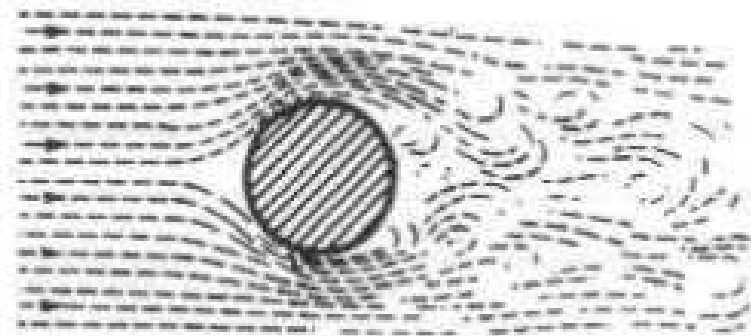


- Streamlining reduces drag by reducing  $F_{D,pressure}$ , at the cost of increasing wetted surface area and  $F_{D,friction}$ .
- Goal is to eliminate flow separation and minimize total drag  $F_D$ .
- Also improves structural acoustics since separation and vortex shedding can excite structural modes.

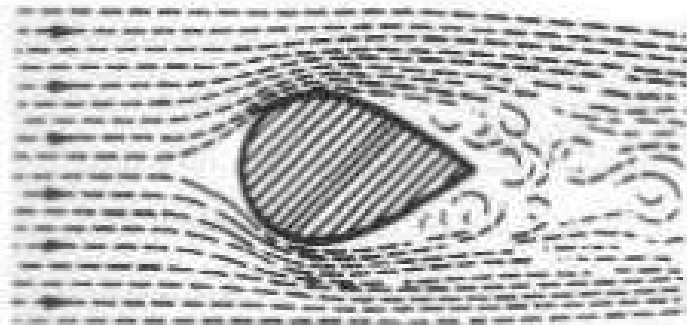
# Streamlining



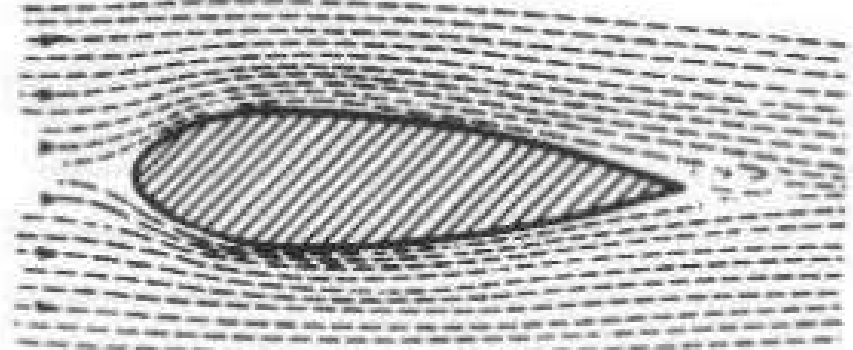
Resistance, 100%



Resistance, 50%



Resistance, 15%



Resistance, 5%

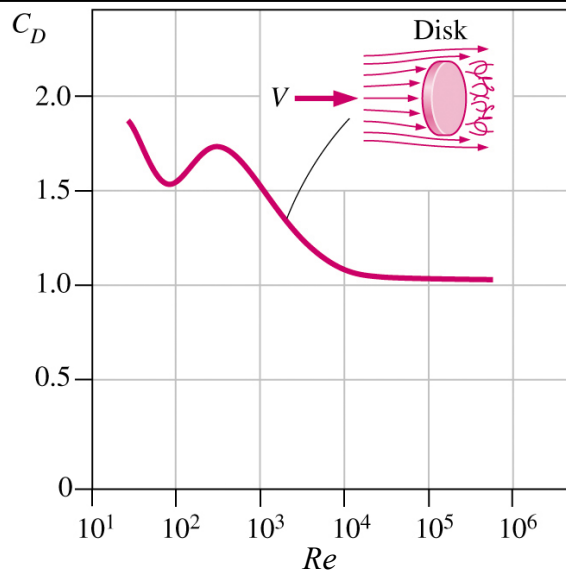
# Streamlining via Active Flow Control



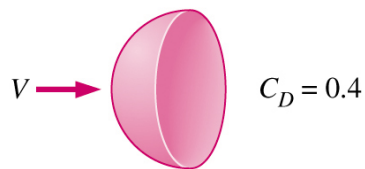
Rounded corners plus pneumatic control (blowing air from slots) reduces drag and improves fuel efficiency for heavy trucks

(Dr. Robert Englar, Georgia Tech Research Institute).

# $C_D$ of Common Geometries



A hemisphere at two different orientations for  $Re > 10^4$



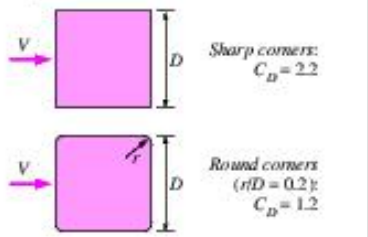
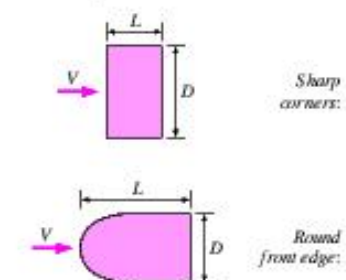
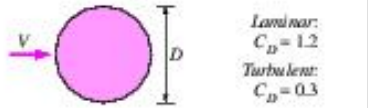
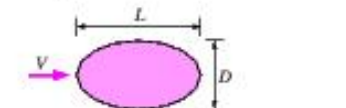
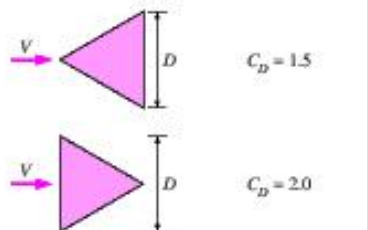
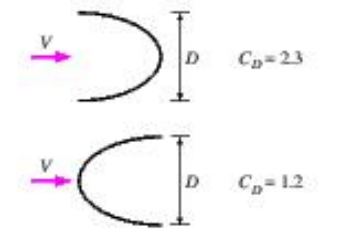
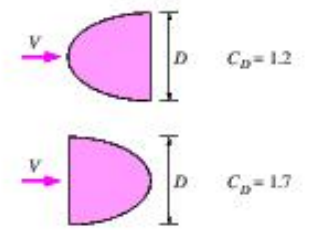
- For many geometries, total drag  $C_D$  is constant for  $Re > 10^4$
- $C_D$  can be very dependent upon orientation of body.
- As a crude approximation, superposition can be used to add  $C_D$  from various components of a system to obtain overall drag. However, there is no mathematical reason (e.g., linear PDE's) for the success of doing this.



# $C_D$ of Common Geometries

**TABLE 11-1**


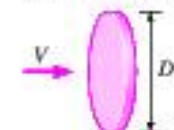


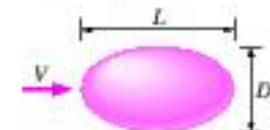
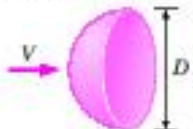
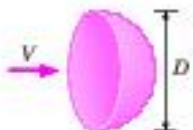
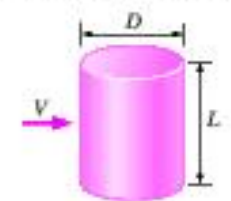
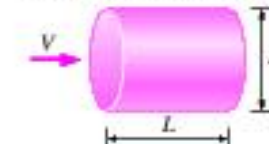
Drag coefficients  $C_D$  of various two-dimensional bodies for  $Re > 10^4$  based on the frontal area  $A = bD$ , where  $b$  is the length in direction normal to the page (for use in the drag force relation  $F_D = C_D A \rho V^2 / 2$  where  $V$  is the upstream velocity)

<p><b>Square rod</b></p>  <p><i>Sharp corners:</i> <math>C_D = 2.2</math></p> <p><i>Round corners</i> (<math>r/D = 0.2</math>): <math>C_D = 1.2</math></p>	<p><b>Rectangular rod</b></p>  <p><i>Sharp corners:</i></p> <table border="1" data-bbox="1161 364 1370 578"> <thead> <tr> <th><math>L/D</math></th> <th><math>C_D</math></th> </tr> </thead> <tbody> <tr> <td>0.0*</td> <td>1.9</td> </tr> <tr> <td>0.1</td> <td>1.9</td> </tr> <tr> <td>0.5</td> <td>2.5</td> </tr> <tr> <td>1.0</td> <td>2.2</td> </tr> <tr> <td>2.0</td> <td>1.7</td> </tr> <tr> <td>3.0</td> <td>1.3</td> </tr> </tbody> </table> <p>* Corresponds to thin plate</p> <table border="1" data-bbox="1161 621 1370 778"> <thead> <tr> <th><math>L/D</math></th> <th><math>C_D</math></th> </tr> </thead> <tbody> <tr> <td>0.5</td> <td>1.2</td> </tr> <tr> <td>1.0</td> <td>0.9</td> </tr> <tr> <td>2.0</td> <td>0.7</td> </tr> <tr> <td>4.0</td> <td>0.7</td> </tr> </tbody> </table> <p><i>Round front edge:</i></p>	$L/D$	$C_D$	0.0*	1.9	0.1	1.9	0.5	2.5	1.0	2.2	2.0	1.7	3.0	1.3	$L/D$	$C_D$	0.5	1.2	1.0	0.9	2.0	0.7	4.0	0.7
$L/D$	$C_D$																								
0.0*	1.9																								
0.1	1.9																								
0.5	2.5																								
1.0	2.2																								
2.0	1.7																								
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0.5	1.2																								
1.0	0.9																								
2.0	0.7																								
4.0	0.7																								
<p><b>Circular rod (cylinder)</b></p>  <p><i>Laminar:</i> <math>C_D = 1.2</math></p> <p><i>Turbulent:</i> <math>C_D = 0.3</math></p>	<p><b>Elliptical rod</b></p>  <table border="1" data-bbox="1123 828 1428 992"> <thead> <tr> <th rowspan="2"><math>L/D</math></th> <th colspan="2"><math>C_D</math></th> </tr> <tr> <th>Laminar</th> <th>Turbulent</th> </tr> </thead> <tbody> <tr> <td>2</td> <td>0.60</td> <td>0.20</td> </tr> <tr> <td>4</td> <td>0.35</td> <td>0.15</td> </tr> <tr> <td>8</td> <td>0.25</td> <td>0.10</td> </tr> </tbody> </table>	$L/D$	$C_D$		Laminar	Turbulent	2	0.60	0.20	4	0.35	0.15	8	0.25	0.10										
$L/D$	$C_D$																								
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2	0.60	0.20																							
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<p><b>Equilateral triangular rod</b></p>  <p><math>C_D = 1.5</math></p> <p><math>C_D = 2.0</math></p>	<p><b>Semicircular shell</b></p>  <p><math>C_D = 2.3</math></p> <p><math>C_D = 1.2</math></p> <p><b>Semicircular rod</b></p>  <p><math>C_D = 1.2</math></p> <p><math>C_D = 1.7</math></p>																								

# $C_D$ of Common Geometries

**TABLE 11-2**

Representative drag coefficients  $C_D$  for various three-dimensional bodies for  $Re > 10^4$  based on the frontal area (for use in the drag force relation  $F_D = C_D A \rho V^2 / 2$  where  $V$  is the upstream velocity)

<p>Cube, <math>A = D^2</math></p>  <p><math>C_D = 1.05</math></p>	<p>Thin circular disk, <math>A = \pi D^2 / 4</math></p>  <p><math>C_D = 1.1</math></p>	<p>Cone (for <math>\theta = 30^\circ</math>), <math>A = \pi D^2 / 4</math></p>  <p><math>C_D = 0.5</math></p>																										
<p>Sphere, <math>A = \pi D^2 / 4</math></p>  <p>Laminar: <math>C_D = 0.5</math> Turbulent: <math>C_D = 0.2</math></p>	<p>Ellipsoid, <math>A = \pi D^2 / 4</math></p>  <table border="1" data-bbox="1275 642 1656 913"> <thead> <tr> <th rowspan="2"><math>L/D</math></th> <th colspan="2"><math>C_D</math></th> </tr> <tr> <th>Laminar</th> <th>Turbulent</th> </tr> </thead> <tbody> <tr> <td>0.75</td> <td>0.5</td> <td>0.2</td> </tr> <tr> <td>1</td> <td>0.5</td> <td>0.2</td> </tr> <tr> <td>2</td> <td>0.3</td> <td>0.1</td> </tr> <tr> <td>4</td> <td>0.3</td> <td>0.1</td> </tr> <tr> <td>8</td> <td>0.2</td> <td>0.1</td> </tr> </tbody> </table>		$L/D$	$C_D$		Laminar	Turbulent	0.75	0.5	0.2	1	0.5	0.2	2	0.3	0.1	4	0.3	0.1	8	0.2	0.1						
$L/D$	$C_D$																											
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0.75	0.5	0.2																										
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<p>Hemisphere, <math>A = \pi D^2 / 4</math></p>  <p><math>C_D = 0.4</math></p>  <p><math>C_D = 1.2</math></p>	<p>Short cylinder, vertical, <math>A = LD</math></p>  <table border="1" data-bbox="1028 985 1180 1242"> <thead> <tr> <th><math>L/D</math></th> <th><math>C_D</math></th> </tr> </thead> <tbody> <tr> <td>1</td> <td>0.6</td> </tr> <tr> <td>2</td> <td>0.7</td> </tr> <tr> <td>5</td> <td>0.8</td> </tr> <tr> <td>10</td> <td>0.9</td> </tr> <tr> <td>40</td> <td>1.0</td> </tr> <tr> <td><math>\infty</math></td> <td>1.2</td> </tr> </tbody> </table> <p>Values are for laminar flow</p>	$L/D$	$C_D$	1	0.6	2	0.7	5	0.8	10	0.9	40	1.0	$\infty$	1.2	<p>Short cylinder, horizontal, <math>A = \pi D^2 / 4</math></p>  <table border="1" data-bbox="1504 985 1656 1213"> <thead> <tr> <th><math>L/D</math></th> <th><math>C_D</math></th> </tr> </thead> <tbody> <tr> <td>0.5</td> <td>1.1</td> </tr> <tr> <td>1</td> <td>0.9</td> </tr> <tr> <td>2</td> <td>0.9</td> </tr> <tr> <td>4</td> <td>0.9</td> </tr> <tr> <td>8</td> <td>1.0</td> </tr> </tbody> </table>	$L/D$	$C_D$	0.5	1.1	1	0.9	2	0.9	4	0.9	8	1.0
$L/D$	$C_D$																											
1	0.6																											
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8	1.0																											

# $C_D$ of Common Geometries

TABLE 11-2 (Continued)

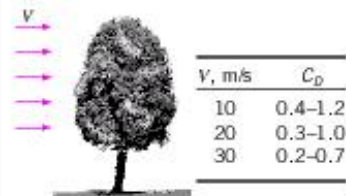
Streamlined body,  $A = \pi D^2/4$



Parachute,  $A = \pi D^2/4$



Tree,  $A =$  frontal area



Person (average)



Standing:  $C_D A = 9 \text{ ft}^2 = 0.84 \text{ m}^2$   
 Sitting:  $C_D A = 6 \text{ ft}^2 = 0.56 \text{ m}^2$

Bikes



Upright:  
 $A = 5.5 \text{ ft}^2 = 0.51 \text{ m}^2$   
 $C_D = 1.1$



$C_D = 0.5$     $C_D = 0.9$



Crouching:  
 $A = 3.9 \text{ ft}^2 = 0.36 \text{ m}^2$   
 $C_D = 0.50$



Racing:  
 $A = 3.9 \text{ ft}^2 = 0.36 \text{ m}^2$   
 $C_D = 0.9$



With fairing:  
 $A = 5.0 \text{ ft}^2 = 0.46 \text{ m}^2$   
 $C_D = 0.12$

Semitrailer,  $A =$  frontal area



Automotive,  $A =$  frontal area



Minivan:  
 $C_D = 0.4$



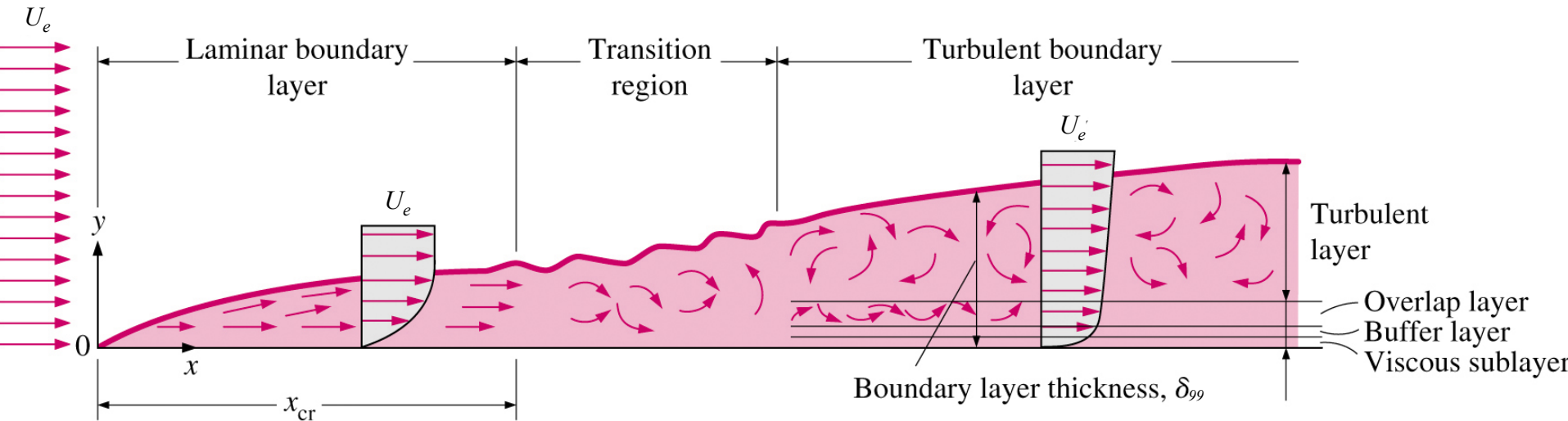
Passenger car:  
 $C_D = 0.3$

High-rise buildings,  $A =$  frontal area



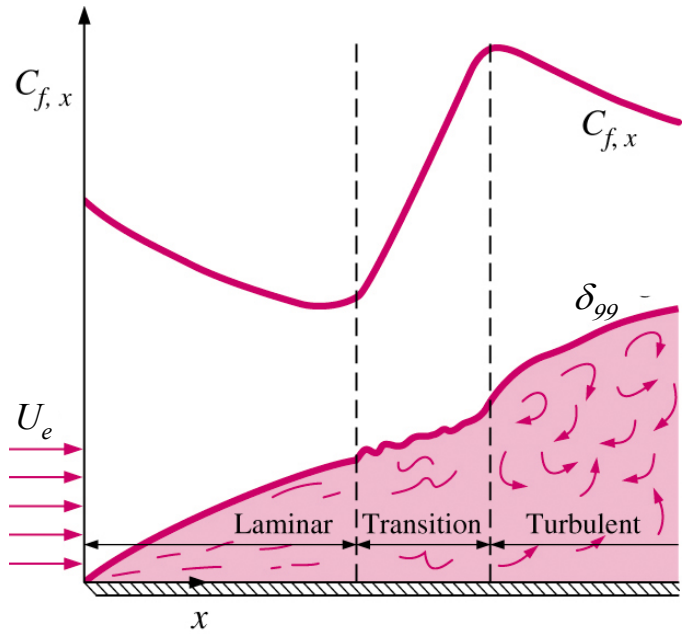
$C_D = 1.4$

# Flat Plate Drag



- Drag on flat plate is solely due to friction created by laminar, transitional, and turbulent boundary layers.

# Flat Plate Drag



## Local friction coefficient

- Laminar:  $C_{f,x} = \frac{0.664}{Re_x^{1/2}}$
- Turbulent:  $C_{f,x} = \frac{0.059}{Re_x^{1/5}}$

## Average friction coefficient

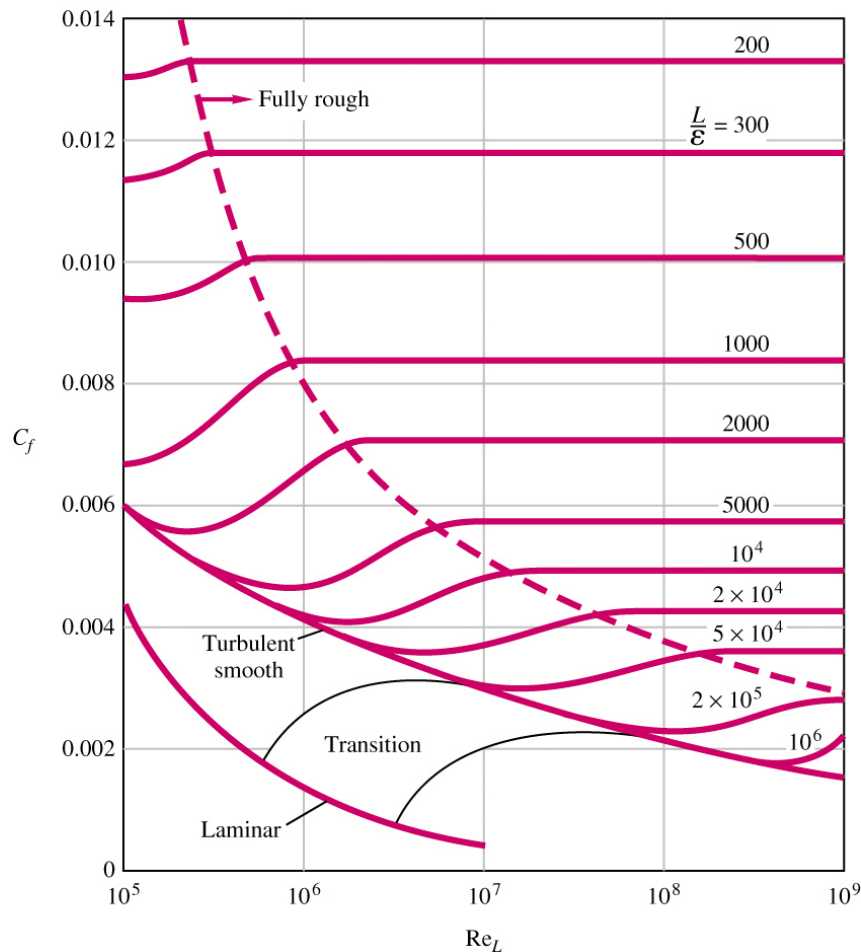
$$C_f = \frac{1}{L} \int_0^L C_{f,x} dx$$

- Laminar:  $C_f = \frac{1.33}{Re_L^{1/2}}$
- Turbulent:  $C_f = \frac{0.074}{Re_L^{1/5}}$

For some cases, plate is long enough for turbulent flow, but not long enough to neglect laminar portion

$$C_f = \frac{1}{L} \left( \int_0^{x_{cr}} C_{f,x,lam} dx + \int_{x_{cr}}^L C_{f,x,turb} dx \right) \quad C_f = \frac{0.075}{Re_L^{1/5}} - \frac{1742}{Re_L}$$

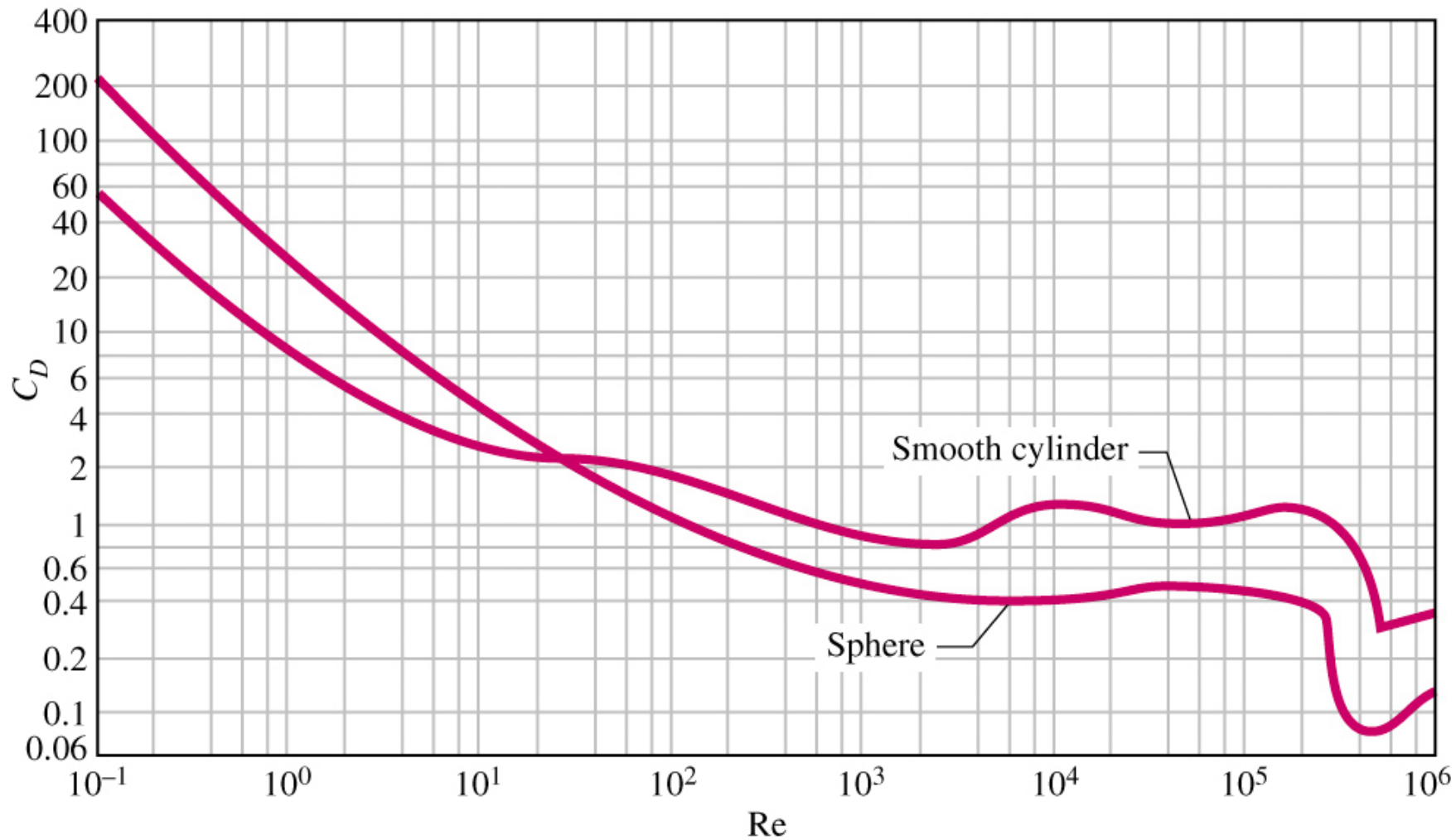
# Effect of Roughness



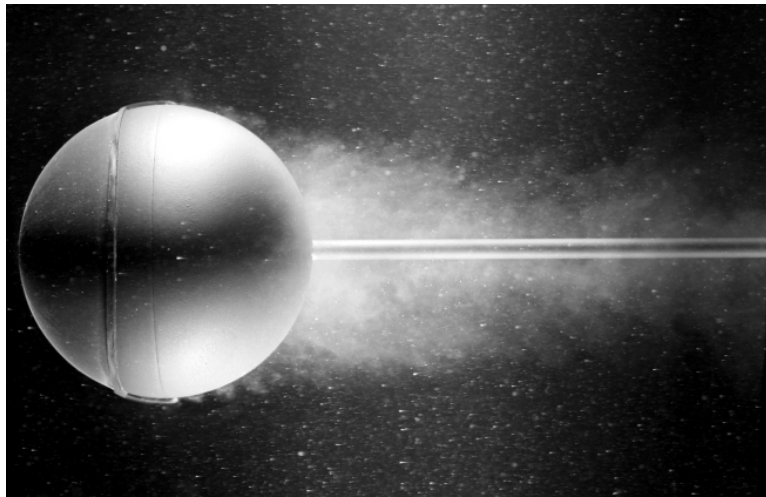
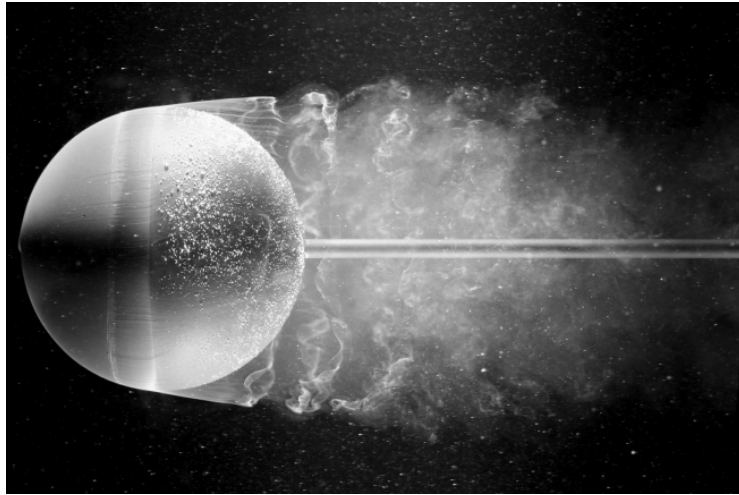
- Similar to Moody Chart for pipe flow
- Laminar flow unaffected by roughness
- Turbulent flow significantly affected:  $C_f$  can increase by 7 times for a given  $Re$

$$C_f = (1.89 - 1.62 \log \frac{\epsilon}{L})^{-2.5}$$

# Cylinder and Sphere Drag



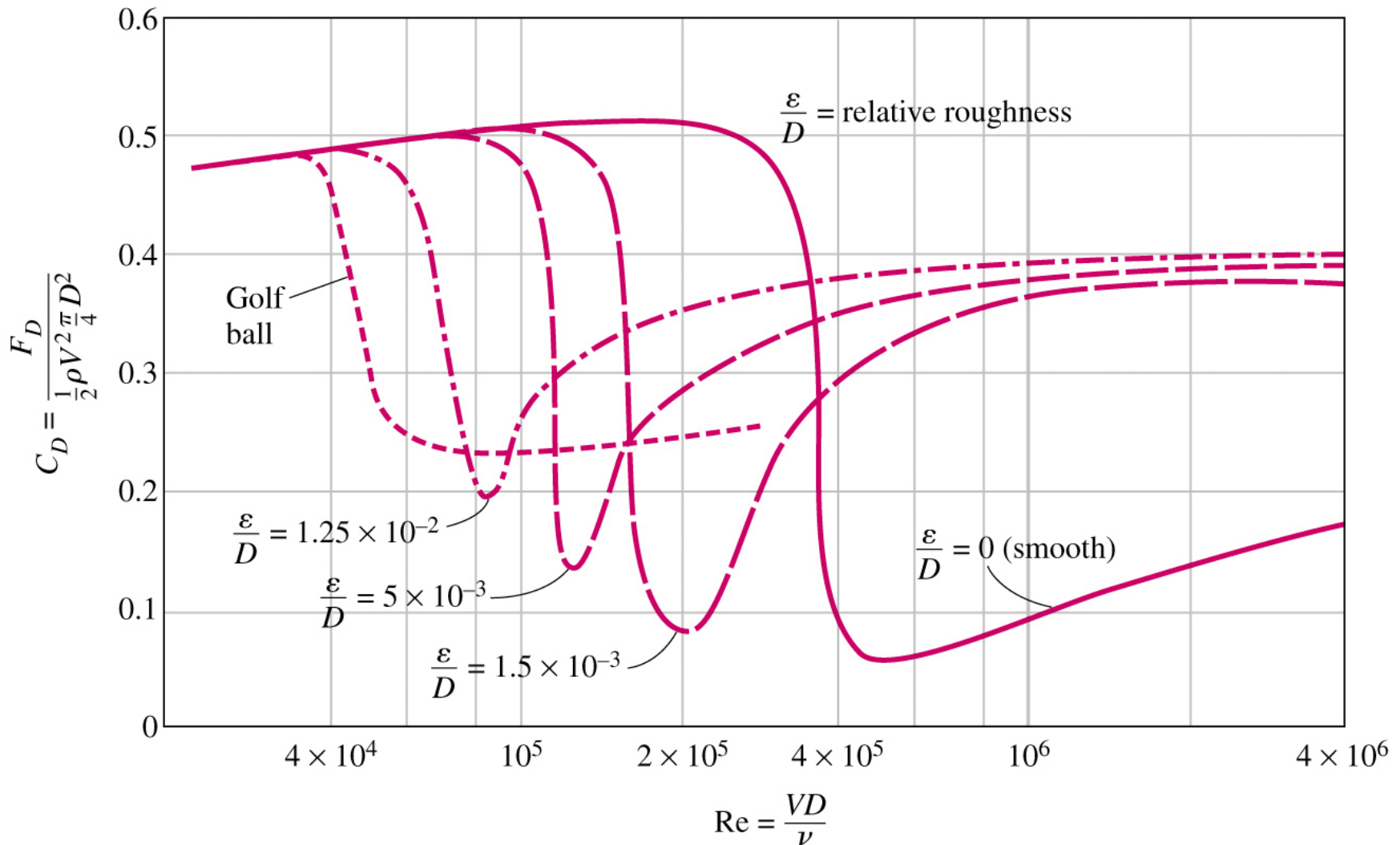
# Cylinder and Sphere Drag



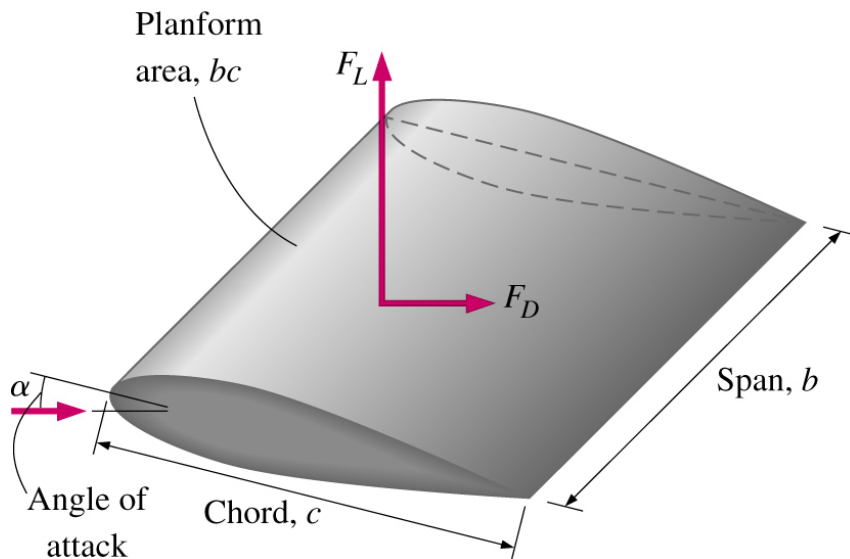
- Flow is strong function of  $Re$ .
- Wake narrows for turbulent flow since TBL (turbulent boundary layer) is more resistant to separation due to adverse pressure gradient.
- $\theta_{\text{sep,turb}} \approx 80^\circ$
- $\theta_{\text{sep,lam}} \approx 140^\circ$



# Effect of Surface Roughness



# Lift



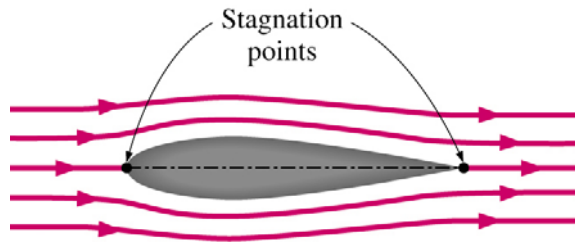
- Lift is the net force (due to pressure and viscous forces) perpendicular to flow direction.

- Lift coefficient

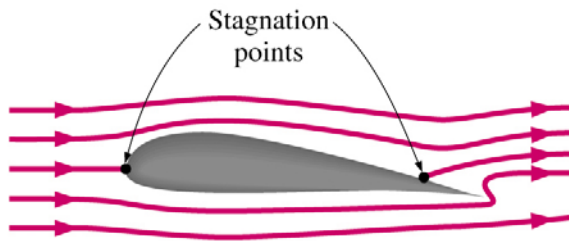
$$C_L = \frac{F_L}{\frac{1}{2}\rho V^2 A}$$

- $A=bc$  is the planform area

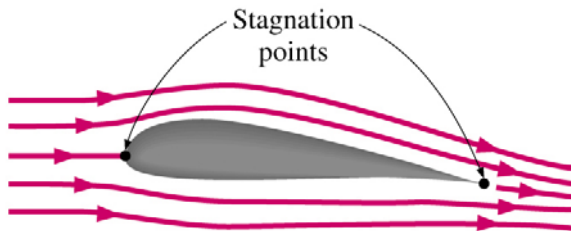
# Computing Lift



(a) Irrotational flow past a symmetrical airfoil (zero lift)



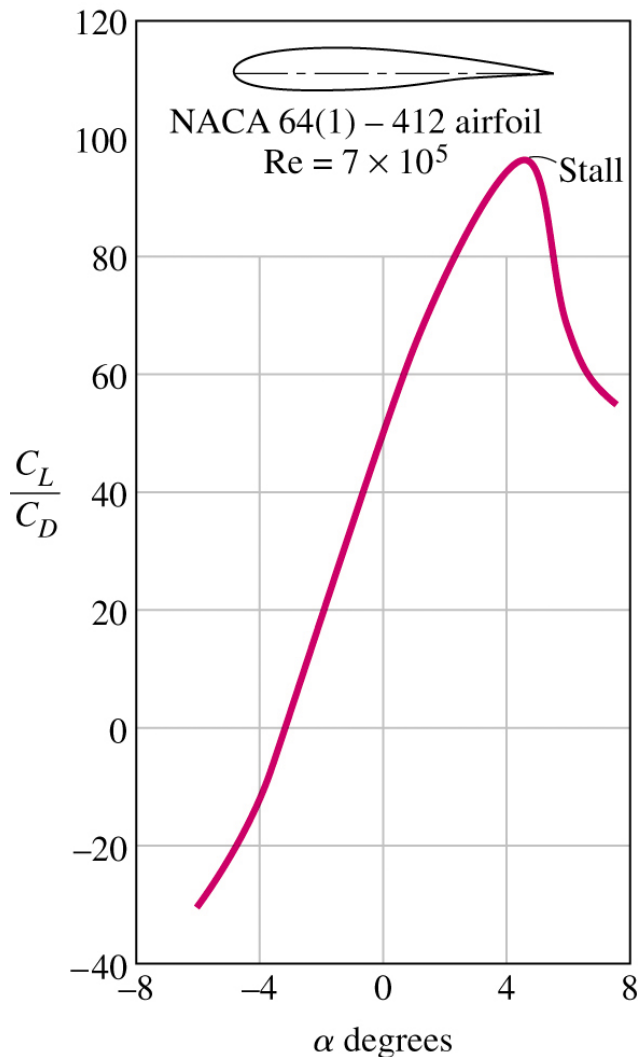
(b) Irrotational flow past a nonsymmetrical airfoil (zero lift)



(c) Actual flow past a nonsymmetrical airfoil (positive lift)

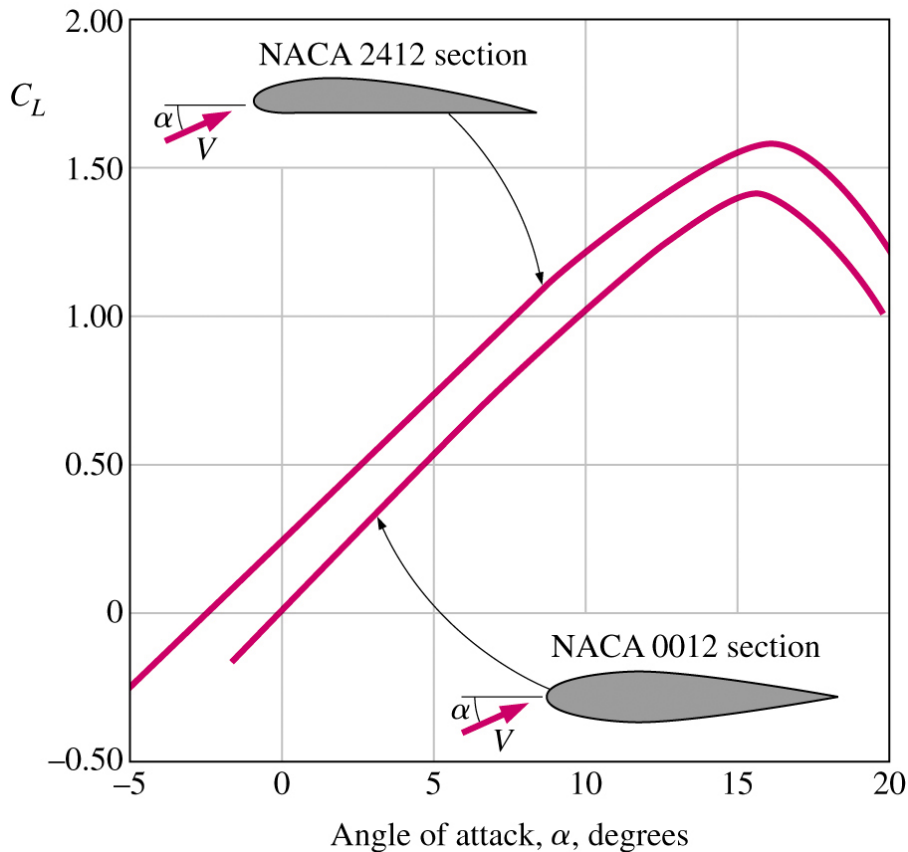
- Potential-flow approximation gives accurate  $C_L$  for angles of attack below stall: boundary layer can be neglected.
- Thin-foil theory: superposition of uniform stream and vortices on mean camber line.
- Java-applet panel codes available online:  
[http://www.aa.nps.navy.mil/~jones/online\\_tools/panel2/](http://www.aa.nps.navy.mil/~jones/online_tools/panel2/)
- **Kutta condition** required at trailing edge: fixes stagnation point at TE.

# Effect of Angle of Attack



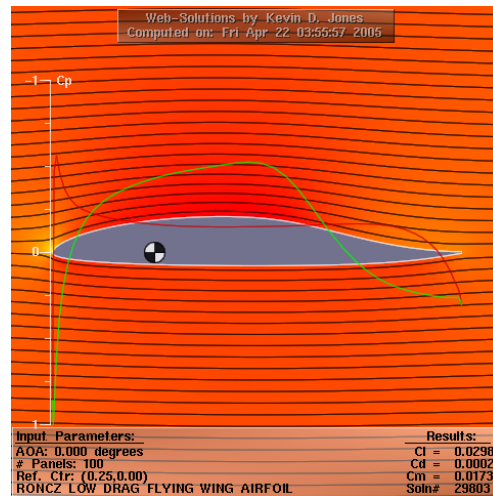
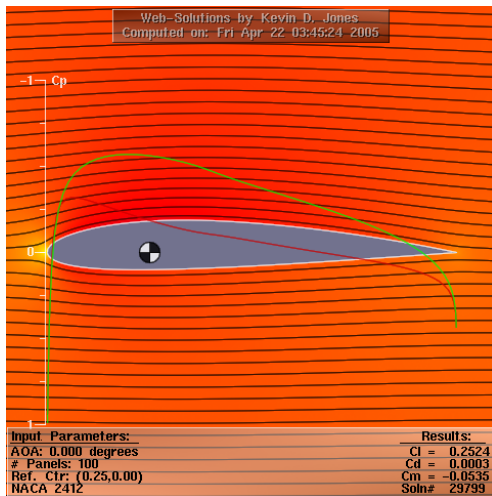
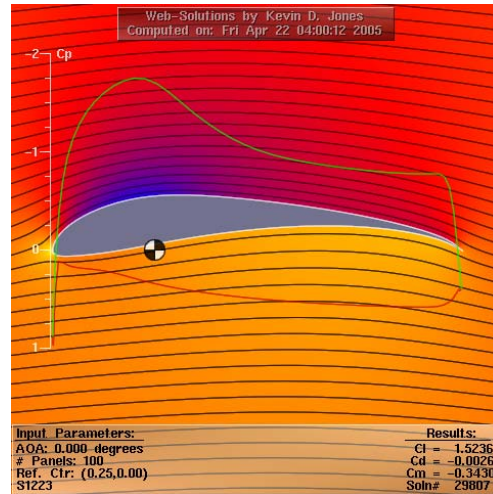
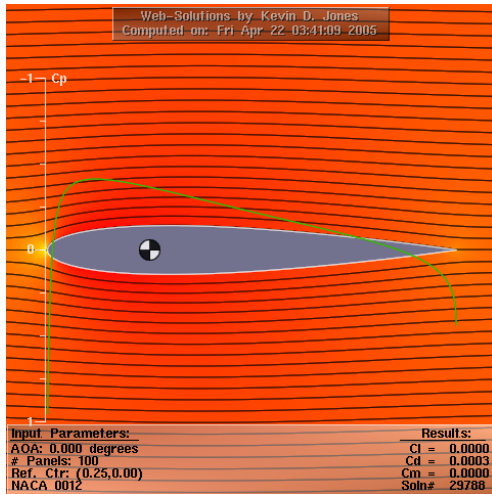
- Thin-foil theory shows that  $C_L \approx 2\pi\alpha$  for  $\alpha < \alpha_{\text{stall}}$
- Therefore, lift increases linearly with  $\alpha$
- Objective for most applications is to achieve maximum  $C_L/C_D$  ratio.
- $C_D$  determined from wind-tunnel or CFD (BLE or NSE).
- $C_L/C_D$  increases (up to order 100) until stall.

# Effect of Foil Shape



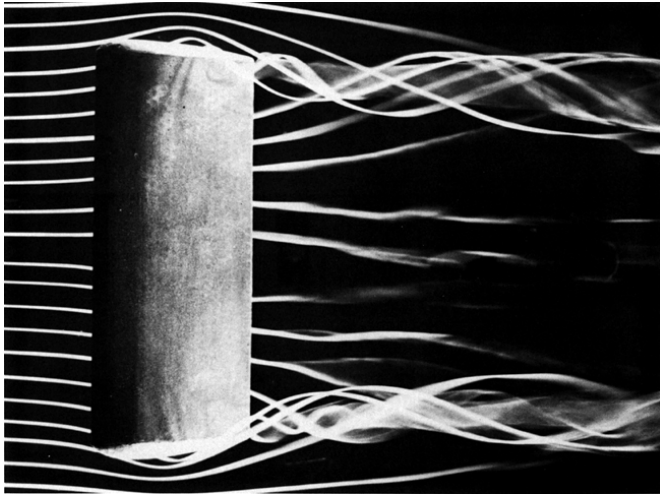
- Thickness and camber influence pressure distribution (and load distribution) and location of flow separation.
- Foil database compiled by Selig (UIUC)  
<http://www.aae.uiuc.edu/m-selig/ads.html>

# Effect of Foil Shape



- Figures from NPS airfoil java applet.
  - Color contours of pressure field
  - Streamlines through velocity field
  - Plot of surface pressure
- Camber and thickness shown to have large impact on flow field.

# End Effects of Wing Tips



- Tip vortex created by leakage of flow from high-pressure side to low-pressure side of wing.
- Tip vortices from heavy aircraft persist far downstream and pose danger to light aircraft. Also sets takeoff and landing separation times at busy airports.

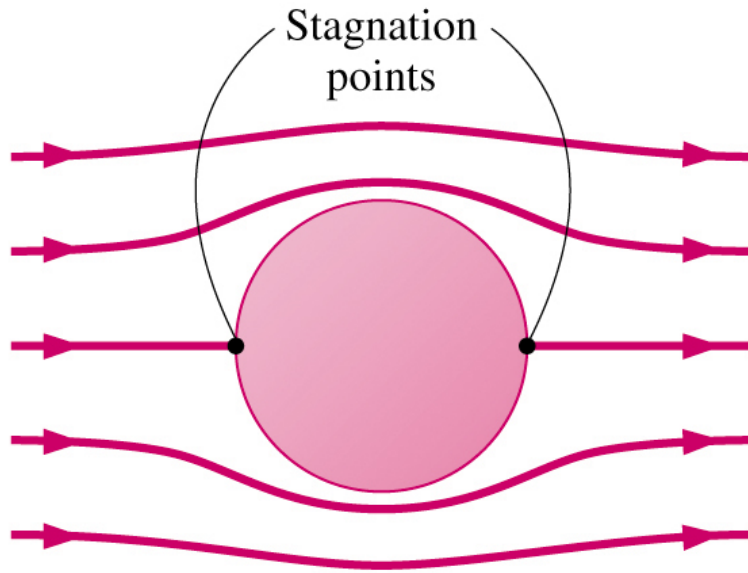
# End Effects of Wing Tips



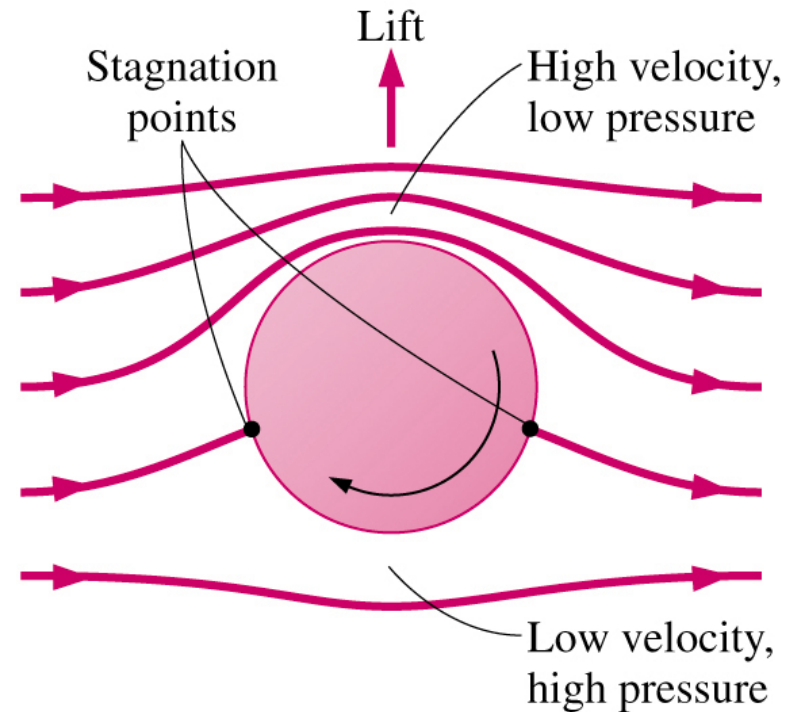
- Tip effects can be reduced by attaching *endplates* or *winglets*.
- Trade-off between reducing induced drag and increasing friction drag.
- Wing-tip feathers on some birds serve the same function.



# Lift Generated by Spinning



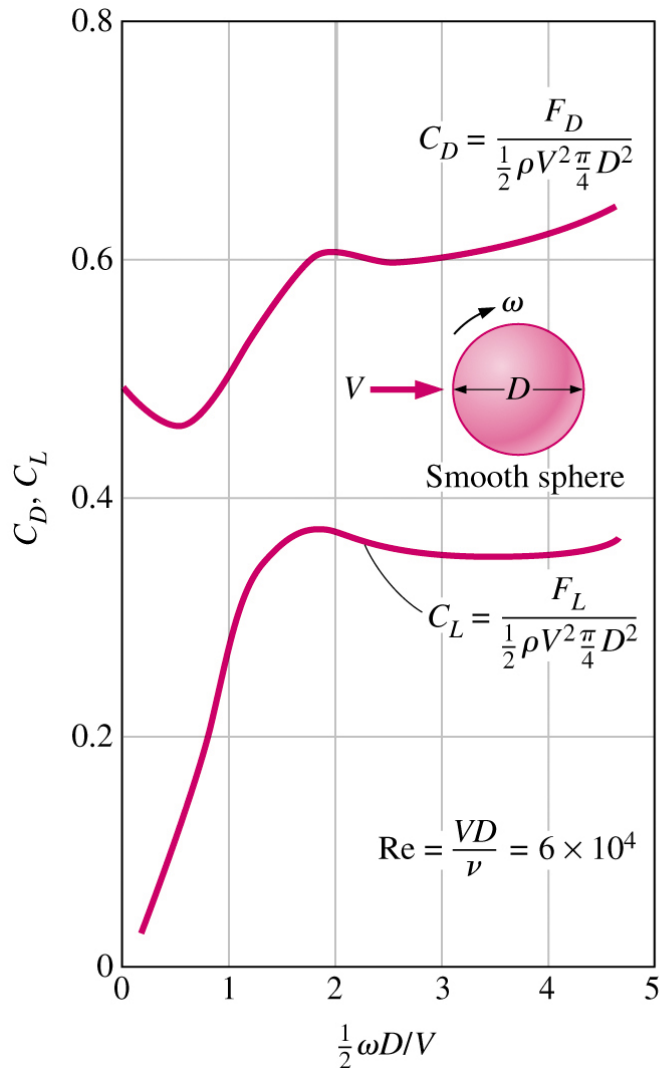
(a) Potential flow over a stationary cylinder



(b) Potential flow over a rotating cylinder

Superposition of **Uniform stream** + **Doublet** + **Vortex**

# Lift Generated by Spinning



- $C_L$  strongly depends on rate of rotation.
- The effect of rate of rotation on  $C_D$  is smaller.
- Baseball, golf, soccer, tennis players utilize spin.
- Lift generated by rotation is called the *Magnus Effect*.